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Model Splitting and First Order Sliding Mode Observers for Estimation and Diagnosis in Vehicle

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Abstract: In this paper a 16 Dof vehicle model is decomposed and used for partial state observation and some inputs estimation. The used sub-models are non linearly coupled and shown to behave well in application. Robust partial state observers with estimation of unknown inputs are developed using First Order Sliding Modes.

Keywords: Vehicles Dynamic; Sliding Modes observer ; Robust nonlinear observers; Robust Estimation; Diagnosis and testing; Coupled Sub-Models; Passive Systems.

1. INTRODUCTION

In literature, many studies deal with vehicle modeling, but model properties are never detailed nor its passivity emphasized. Vehicle dynamics can be represented by approximate models which are either too much simplified to be realistic or complex and have a variable structure (M'sirdi et al. [2007a]). This kind of systems are composed with many passively coupled subsystems: wheels, motor and braking control system, suspensions, steering, more and more inboard and embedded electronics. There are several non linear parts, which are coupled. These coupling may be time varying and non stationary (M'sirdi et al. [2007c]). Approximations have to be made carefully regarding to the desired application.

In previous works a good nominal vehicle model with 16 DOF have been developed and validated for a French vehicle type (P406) (ElHadri et al. [2000]). Several interesting applications was successful and have been evaluated by use of this model before actual results (M'sirdi et al. [2004], Rabhi et al. [2004]). We have also considered this modeling for estimation of unknown inputs (M'sirdi et al. [2006b]), interaction parameters and exchanges with environment (M'sirdi et al. [2004]). This approach has been used successfully also for heavy vehicles (M'sirdi et al. [2006a]).

In this paper this model is revisited and structured for estimation of inputs and diagnosis. We split the model in five subsystems (M'sirdi et al. [2007b]), regrouped in 3 blocks and then show and justify the rationale behind the successful splitting. The subsystems and the overall system obey the passivity property. This feature, like in Bond Graphs modeling emphasize the energy flow and exchanges between the system parts and also with the

environment. After the structure and model analysis, we consider estimation of the partial states for diagnosis and motion control in the vehicle. Robust estimations are necessary to be able to obtain good evaluation of the driving situation at each time instant.

2. NOMINAL VEHICLE MODELING

Let us consider the fixed reference frame R and represent the vehicle by the scheme of figure (1) (M'sirdi et al. [2007a], M'sirdi et al. [2007b], M'sirdi et al. [2007c]). The generalized coordinates vector $q \in R^{16}$ is defined as :

$$q^T = [x, y, z, \theta_x, \theta_y, \theta_z, q_{31}, q_{32}, q_{33}, q_{34}, \delta_3, \delta_4, \varphi_1, \varphi_2, \varphi_3, \varphi_4]$$

where x, y , and z represent displacements. Angles of roll, pitch and yaw are θ_x, θ_y and θ_z respectively. The suspensions elongations are noted q_{3i} : ($i = 1..4$). δ_i : stands for the steering angles ($i = 3, 4$). φ_i : are angles of wheels rotations ($i = 1..4$). $\dot{q}, \ddot{q} \in R^{16}$ are respectively velocities and corresponding accelerations.

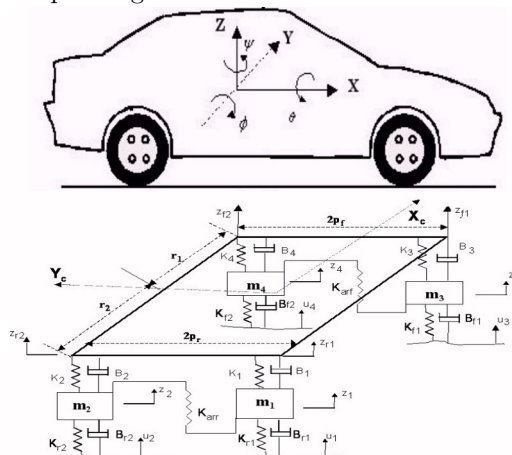


Fig. 1. Vehicle dynamics and reference frames

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2.1 Global Dynamics Model

The Nominal model of the vehicle with uncertainties is developed in assuming the car body rigid and pneumatic contact permanent and reduced to one point for each wheel. The vehicle motion can be described by the passive model: (M'sirdi et al. [2004])

$$\tau = M(q)\ddot{q} + C(q, \dot{q})\dot{q} + V(q, \dot{q}) + \eta_o(t, q, \dot{q}) \quad (1)$$

$$\tau = \Gamma_e + \Gamma = \Gamma_e + J^T F \quad (2)$$

The input torque τ is composed by a part produced by the actuators, which can be assumed to be given by some feedback function and reaction of the road. In equation (2), we remark that there are control inputs from driving and external inputs coming from exchanges with environment (road reactions).

The matrix $M(q)$, of dimension 16x16, is Symmetric Positive Definite (SPD) inertia matrix and $C(q, \dot{q})$, of dimension too 16x16, is matrix of coriolis and centrifugal forces. (see details of the two matrix $M(q)$ and $C(q, \dot{q})$ in the appendix A)(ElHadri et al. [2000] and Canudas-deWit et al. [2003])

The vector $V(q, \dot{q}) = \xi(K_v \dot{q} + K_p q) + G(q)$ are suspensions and gravitation forces (with K_v and K_p are respectively damping and stiffness matrices, $G(q)$ is the gravity term and ξ is equal to unity when the corresponding wheel is in contact with the ground and zero if not). $\eta_o(t, x_1, x_2)$ are the uncertainties and neglected dynamics.

The vector Γ_e represent external inputs for perturbations. The environment reactions are represented by $J^T F$ where J is the Jacobian matrix (see detail in appendix A), of dimensions 16x12, and F is the input forces vector acting on the wheels, it has 12 components (longitudinal F_{xi} , lateral F_{yi} and normal F_{zi} , $i = 1..4$): (Canudas-deWit et al. [2003])

$$F = [F_{x1}, F_{y1}, F_{z1}, F_{x2}, F_{y2}, F_{z2}, F_{x3}, F_{y3}, F_{z3}, F_{x4}, F_{y4}, F_{z4}]$$

2.2 Coupled sub models

We can split the previous model (1) while considering: the inertia matrix as composed by five lines and five column as follows and split positions in five parts by writing $q^T = [q_1^T, q_2^T, q_3^T, q_4^T, q_5^T]$:

$$\begin{aligned} q_1^T &= [x, y, z] \\ q_2^T &= [\theta_x, \theta_y, \theta_z] \\ q_3^T &= [q_{31}, q_{32}, q_{33}, q_{34}] \\ q_4^T &= [\delta_3, \delta_4] \\ q_5^T &= [\varphi_1, \varphi_2, \varphi_3, \varphi_4] \end{aligned} \quad (3)$$

By considering too the vectors Γ_e , $V(q, \dot{q})$ and $\eta_o(t, x_1, x_2)$ are splitting as follows :

$$\Gamma_e = [0 \ 0 \ 0 \ \Gamma_{e4} \ \Gamma_{e5}]^T \quad (4)$$

$$V(q, \dot{q}) = [V_1 \ V_2 \ V_3 \ V_4 \ V_5]^T \quad (5)$$

$$\eta_o(t, x_1, x_2) = [\eta_1 \ \eta_2 \ \eta_3 \ \eta_4 \ \eta_5]^T \quad (6)$$

The 16 Degrees of Freedom model is then equivalent to: (M'sirdi et al. [2008], M'sirdi et al. [2007c])

$$\begin{aligned} \begin{bmatrix} 0 \\ 0 \\ 0 \\ \Gamma_{e4} \\ \Gamma_{e5} \end{bmatrix} + \begin{bmatrix} J_1^T \\ J_2^T \\ J_3^T \\ 0 \\ 0 \end{bmatrix} F &= \begin{bmatrix} \bar{M}_{11} & \bar{M}_{12} & \bar{M}_{13} & 0 & 0 \\ \bar{M}_{21} & \bar{M}_{22} & \bar{M}_{23} & \bar{M}_{24} & \bar{M}_{25} \\ \bar{M}_{31} & \bar{M}_{32} & \bar{M}_{33} & 0 & 0 \\ 0 & \bar{M}_{42} & 0 & \bar{M}_{44} & 0 \\ 0 & \bar{M}_{52} & 0 & 0 & \bar{M}_{55} \end{bmatrix} \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \\ \ddot{q}_3 \\ \ddot{q}_4 \\ \ddot{q}_5 \end{bmatrix} \\ &+ \begin{bmatrix} 0 & \bar{C}_{12} & \bar{C}_{13} & 0 & 0 \\ 0 & \bar{C}_{22} & \bar{C}_{23} & \bar{C}_{24} & \bar{C}_{25} \\ 0 & \bar{C}_{32} & \bar{C}_{33} & 0 & 0 \\ 0 & \bar{C}_{42} & 0 & 0 & \bar{C}_{45} \\ 0 & \bar{C}_{52} & 0 & \bar{C}_{54} & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \end{bmatrix} + \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \end{bmatrix} + \begin{bmatrix} \eta_1 \\ \eta_2 \\ \eta_3 \\ \eta_4 \\ \eta_5 \end{bmatrix} \end{aligned}$$

The model (1) is then split in 5 equations corresponding respectively to chassis translations, Chassis rotations, Suspensions elongations, wheel steering and wheel rotations, with as positions q_1, q_2, q_3, q_4 and q_5 . This leads us to the body's translations dynamics described by equation (7):

$$F_T = J_1^T F \quad (7)$$

$$= \bar{M}_{11}\ddot{q}_1 + \bar{M}_{12}\ddot{q}_2 + \bar{M}_{13}\ddot{q}_3 + \bar{C}_{12}\dot{q}_2 + \bar{C}_{13}\dot{q}_3 + V_1 + \eta_1$$

Rotations and orientation motions of the body are in (8):

$$F_R = J_2^T F \quad (8)$$

$$= \bar{M}_{21}\ddot{q}_1 + \bar{M}_{22}\ddot{q}_2 + \bar{M}_{23}\ddot{q}_3 + \bar{M}_{24}\ddot{q}_4 + \bar{M}_{25}\ddot{q}_5 + \bar{C}_{22}\dot{q}_2 + \bar{C}_{23}\dot{q}_3 + \bar{C}_{24}\dot{q}_4 + \bar{C}_{25}\dot{q}_5 + V_2 + \eta_2$$

The suspension dynamics are in (9):

$$F_S = J_3^T F \quad (9)$$

$$= \bar{M}_{31}\ddot{q}_1 + \bar{M}_{32}\ddot{q}_2 + \bar{M}_{33}\ddot{q}_3 + \bar{C}_{32}\dot{q}_2 + \bar{C}_{33}\dot{q}_3 + V_3 + \eta_3$$

The rest in (10-11) is for wheels steering and rotations:

$$\Gamma_{e4} = \bar{M}_{42}\ddot{q}_2 + \bar{M}_{44}\ddot{q}_4 + \bar{C}_{42}\dot{q}_2 + \bar{C}_{45}\dot{q}_5 + V_4 + \eta_4 \quad (10)$$

$$\Gamma_{e5} = \bar{M}_{52}\ddot{q}_2 + \bar{M}_{55}\ddot{q}_5 + \bar{C}_{52}\dot{q}_2 + \bar{C}_{54}\dot{q}_4 + V_5 + \eta_5 \quad (11)$$

It is worthwhile to note that until now there are no approximations when considering the 5 equations. Approximations will be made when neglecting the coupling terms η_c^i . In the previous expressions, we remark that splitting the model is helpful, when using reduced models, to identify what is neglected regard to our proposed nominal model with 16 DoF. η_c^i are coupling terms du to connections with the other sub systems. We can verify that these terms are bounded such and as $|\eta_c^i| < k_i \forall t, i = (1..5)$.

$$\begin{aligned} \Sigma_{11} : \dot{q}_1 &= f_1(q_1, \dot{q}_1, F_T) + \eta_c^1 \\ \Sigma_{12} : \dot{q}_2 &= f_2(q_2, \dot{q}_2, F_R) + \eta_c^2 \\ \Sigma_2 : \dot{q}_3 &= f_3(q_3, \dot{q}_3, F_S) + \eta_c^3 \\ \Sigma_{31} : \dot{q}_4 &= f_4(q_4, \dot{q}_4, \Gamma_{e4}) + \eta_c^4 \\ \Sigma_{32} : \dot{q}_5 &= f_5(q_5, \dot{q}_5, \Gamma_{e5}) + \eta_c^5 \end{aligned} \quad (12)$$

This can be presented as subsystems Σ_{11} , Σ_{12} , Σ_2 , Σ_{31} and Σ_{32} corresponding respectively to chassis translations, rotations, suspensions elongations, wheels steering and rotations. The scheme of figure (2) represents the various blocks of the model that we develop them in the following part. The two subsystems, Σ_{11} and Σ_{12} , represents together the dynamics of the chassis noted, Σ_1 . The two subsystems, Σ_{31} and Σ_{32} , us give the wheels dynamics, noted Σ_3 .

Dynamics of the chassis Σ_1 : From the global system equations we take the two first equations (7) and (8) for chassis translations and rotations.

$$\begin{bmatrix} F_T \\ F_R \end{bmatrix} = \begin{bmatrix} \bar{M}_{11} & \bar{M}_{12} \\ \bar{M}_{21} & \bar{M}_{22} \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} + \begin{bmatrix} \bar{C}_{12} \\ \bar{C}_{22} \end{bmatrix} \dot{q}_2 + \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} + \begin{bmatrix} \eta_c^1 \\ \eta_c^2 \end{bmatrix}$$

Where the coupling terms, η_c^1 and η_c^2 are giving by:

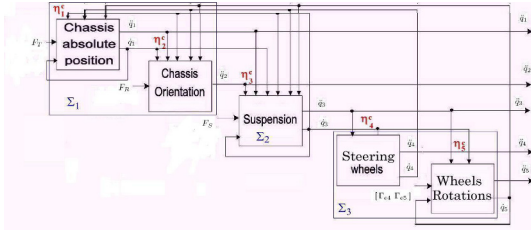


Fig. 2. Five sub models with Coupling terms

$$\eta_c^1 = \bar{M}_{13}\dot{q}_3 + \bar{C}_{13}\dot{q}_3 + \eta_1 \quad (13)$$

$$\eta_c^2 = \bar{M}_{23}\dot{q}_3 + \bar{M}_{24}\dot{q}_4 + \bar{M}_{25}\dot{q}_5 + \bar{C}_{23}\dot{q}_3 + \bar{C}_{24}\dot{q}_4 + \bar{C}_{25}\dot{q}_5 + \eta_2$$

By choosing $x_{11} = (q_1, q_2)$ and $x_{12} = (\dot{q}_1, \dot{q}_2)$, the equivalent state space representation can be written:

$$\begin{cases} \dot{x}_{11} = x_{12} \\ \dot{x}_{12} = M_1^{-1}(J_{12}^T F - C_1 x_{12} - V_{12} - \nu_1) \\ y_1 = h(x_{11}, x_{12}) \end{cases} \quad (14)$$

Where $M_1 = \begin{bmatrix} \bar{M}_{11} & \bar{M}_{12} \\ \bar{M}_{21} & \bar{M}_{22} \end{bmatrix}$, $C_1 = \begin{bmatrix} \bar{C}_{12} \\ \bar{C}_{22} \end{bmatrix}$, $J_{12}^T = \begin{bmatrix} J_1^T \\ J_2^T \end{bmatrix}$, $V_{12} = \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$ and $\mu_1 = \begin{bmatrix} \eta_c^1 \\ \eta_c^2 \end{bmatrix}$ are respectively the reduced inertia matrix (SPD), the reduced matrix of Coriolis and Centrifugal forces, the reduced Jacobian matrix and the vector of suspensions and gravitation forces associated to the two subsystems and the coupling term had by dynamics of the other subsystems.

Suspensions Dynamics Σ_2 : We interest now in the dynamics suspensions gives by the third equation (9) from the global one.

$$F_S = \bar{M}_{33}\ddot{q}_3 + \bar{C}_{33}\dot{q}_3 + V_3 + \eta_c^3 \quad (15)$$

Where \bar{M}_{33} is the inertia matrix associated to subsystem Σ_2 , it is SPD. The coupling term η_c^3 is giving by:

$$\eta_c^3 = \bar{M}_{31}\ddot{q}_1 + \bar{M}_{32}\ddot{q}_2 + \bar{C}_{32}\dot{q}_2 + \eta_3 \quad (16)$$

Let $x_2 = (x_{21}, x_{22}) = (q_3, \dot{q}_3)$, the state space representation of the subsystem Σ_2 is then:

$$\begin{cases} \dot{x}_{21} = x_{22} \\ \dot{x}_{22} = \bar{M}_{33}^{-1}(J_3^T F - \bar{C}_{33}x_{22} - V_3 - \mu_2) \\ y_2 = h(x_2) \end{cases} \quad (17)$$

Where $\mu_2 = \eta_c^3$

Wheels dynamics Σ_3 : The wheels dynamics are given by the wheels steering of the two front wheels (Σ_{31}), and the wheels rotations of the four wheels (Σ_{32}). Then we can write the fourth equation (10) and the five (11) of the model in the following form:

$$\Gamma_{e4} = \bar{M}_{44}\ddot{q}_4 + \bar{C}_{45}\dot{q}_5 + V_4 + \eta_c^4 \quad (18)$$

$$\Gamma_{e5} = \bar{M}_{55}\ddot{q}_5 + \bar{C}_{54}\dot{q}_4 + V_5 + \eta_c^5 \quad (19)$$

The coupling terms η_c^4 and η_c^5 of the two subsystem are giving by the following equations:

$$\eta_c^4 = \bar{M}_{42}\ddot{q}_2 + \bar{C}_{42}\dot{q}_2 + \eta_4 \quad (20)$$

$$\eta_c^5 = \bar{M}_{52}\ddot{q}_2 + \bar{C}_{52}\dot{q}_2 + \eta_5 \quad (21)$$

Then we can write the equations (18 and 19) in the following form:

$$\begin{bmatrix} \Gamma_{e4} \\ \Gamma_{e5} \end{bmatrix} = \begin{bmatrix} \bar{M}_{44} & 0 \\ 0 & \bar{M}_{55} \end{bmatrix} \begin{bmatrix} \ddot{q}_4 \\ \ddot{q}_5 \end{bmatrix} + \begin{bmatrix} 0 & \bar{C}_{45} \\ \bar{C}_{54} & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_4 \\ \dot{q}_5 \end{bmatrix} + \begin{bmatrix} V_4 + \eta_c^4 \\ V_5 + \eta_c^5 \end{bmatrix}$$

By choosing $x_{31} = (q_4, q_5)$ and $x_{32} = (\dot{q}_4, \dot{q}_5)$, the equivalent state space representation can be written:

$$\begin{cases} \dot{x}_{31} = x_{32} \\ \dot{x}_{32} = M_3^{-1}(\Gamma_{e45} - C_3 x_{32} - V_{45} - \mu_3) \\ y_3 = h(x_{31}, x_{32}) \end{cases} \quad (22)$$

Where $M_3 = \begin{bmatrix} \bar{M}_{44} & 0 \\ 0 & \bar{M}_{55} \end{bmatrix}$, $C_3 = \begin{bmatrix} 0 & \bar{C}_{45} \\ \bar{C}_{54} & 0 \end{bmatrix}$, $\Gamma_{e45} = \begin{bmatrix} \Gamma_{e4} \\ \Gamma_{e5} \end{bmatrix}$, $V_{45} = \begin{bmatrix} V_4 \\ V_5 \end{bmatrix}$ and $\mu_3 = \begin{bmatrix} \eta_c^4 \\ \eta_c^5 \end{bmatrix}$ are respectively the reduced inertia matrix (SPD), the reduced matrix of Coriolis and Centrifugal forces, the reduced external inputs vector and the vector of suspensions and gravitation forces associated to the two subsystems and the coupling term had by dynamics of the other subsystems.

2.3 Simulation Results

In order to justify and validate the splitting of the model vehicle applied in the precedent section, we give some simulation results obtained while using a car simulator (SimK106N). The validation of this simulator was made for the laboratory LCPC of Nantes by an instrumented car (peugeot 406). Then we use two steering angle. The figure (3) and (4) represents the various coupling terms by choosing respectively square and sinusoidal steering. We notice that all the coupling terms (μ_1, μ_2, μ_3) and its squares ($\mu_1^2, \mu_2^2, \mu_3^2$) are almost null.

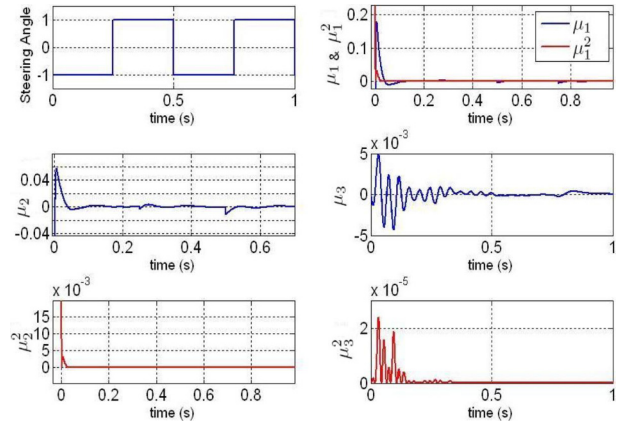


Fig. 3. The Coupling terms for square steering

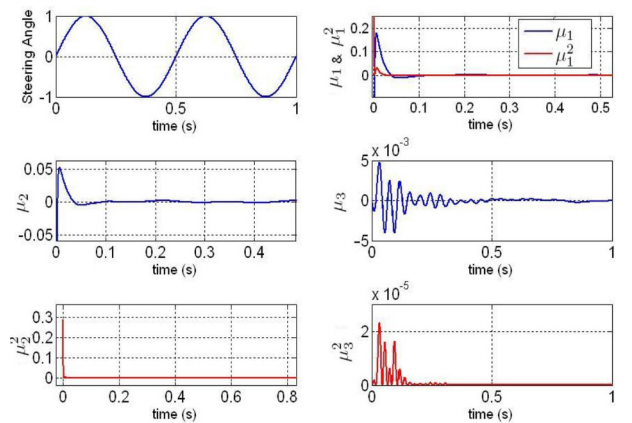


Fig. 4. The Coupling terms for sinusoidal steering

3. FIRST ORDER SLIDING MODE OBSERVERS (FOSM)

The Sliding mode technique is an attractive approach for robustness (Filippov [1988], Utkin et al. [1999]). In this part we will use a First Order Sliding Mode (FOSM) to observe the coordinates vector q_i for each subsystem and to estimate the input forces vector F . To estimate the various coordinates vector (q_i), its derivative (\dot{q}_i) and the forces vector F , we propose in this section to develop an observer based on the First Order Sliding Mode approach followed by an estimator. This approach is robust versus the model and the parameters uncertainties for state estimation and is able to reject perturbations and uncertainties effects.

3.1 Observer for the chassis Dynamics Σ_1 :

By using the state space representation (14) for the subsystem Σ_1 , we propose the following sliding mode observer giving the estimates \hat{x}_{11} , \hat{x}_{12} in two steps:

$$\begin{cases} \dot{\hat{x}}_{11} = \hat{x}_{12} - \Lambda_{11} \text{sign}(\hat{x}_{11} - x_{11}) \\ \dot{\hat{x}}_{12} = M_1^{-1}(J_{12}^T \hat{F} - C_1 \hat{x}_{12} - V_{12} - \mu_1) - \Lambda_{12} \text{sign}(\tilde{x}_{11}) \\ \dot{\hat{F}} = -P_1 \Lambda_{13} \text{sign}(\hat{x}_{11} - x_{11}) \end{cases} \quad (23)$$

Where $P_1 \in R^{12 \times 12}$ is a positive definite matrix and Λ_{11} , Λ_{12} , Λ_{13} are observer gains to be adjusted for convergence, \hat{F} is an a priori estimation of the forces and sign is the vector of sign_i function ($i = 1..6$). For convergence analysis, we have to express the state estimation error ($\tilde{x}_{11} = \hat{x}_{11} - x_{11}$) dynamics equation. Then the equations (14), (23) give the observation error dynamics:

$$\begin{cases} \dot{\tilde{x}}_{11} = \tilde{x}_{12} - \Lambda_{11} \text{sign}(\tilde{x}_{11}) \\ \dot{\tilde{x}}_{12} = M_1^{-1}(J_{12}^T \tilde{F} - C_1 \tilde{x}_{12}) - \Lambda_{12} \text{sign}(\tilde{x}_{11}) \\ \dot{\tilde{F}} = -P_1 \Lambda_{13} \text{sign}(\tilde{x}_{11}) \end{cases} \quad (24)$$

Where $\tilde{x}_{12} = \hat{x}_{12} - x_{12}$ and $\tilde{F} = \hat{F} - F$. These can be assumed bounded owing to fact that all involved terms are either estimates or come from a passive mechanical part of the system and $|\mu_1| < \kappa_0 \forall t$. The Lyapunov function $V_1 = \frac{1}{2} \tilde{x}_{11}^T \tilde{x}_{11}$, help to show that the sliding surface $\tilde{x}_{11} = 0$ is attractive surface if $\dot{V}_1 < 0$:

$$\dot{V}_1 = \tilde{x}_{11}^T (\tilde{x}_{12} - \Lambda_{11} \text{sign}(\tilde{x}_{11})) \quad (25)$$

If we choose $\Lambda_{11} = \text{diag}(\lambda_{11}^i)$ such as $|\tilde{x}_{12}^i| < \lambda_{11}^i$ (for $i = 1, \dots, 3$), the convergence in finite time (t_0) for the subsystem state is obtained: \hat{x}_{11} goes to x_{11} in finite time t_0 , so $\dot{\tilde{x}}_{11} = 0 \forall t > t_0$. Then we obtain a reduced dynamic for the estimation error:

$$\dot{\tilde{x}}_{12} = M_1^{-1} J_{12}^T \tilde{F} - \Lambda_{12} \Lambda_{11}^{-1} \tilde{x}_{12} \quad (26)$$

$$\dot{\tilde{F}} = -P_1 \Lambda_{13} \Lambda_{11}^{-1} \tilde{x}_{12} \quad (27)$$

For the second step of the convergence proof, consider $V_2(\tilde{x}_{12}, \tilde{F}) = \frac{1}{2} \tilde{x}_{12}^T \tilde{x}_{12} + \frac{1}{2} \tilde{F}^T P_1^{-1} \tilde{F}$ then $\dot{V}_2(\tilde{x}_{12}, \tilde{F})$ becomes if we let $\Lambda_{13} = (M_1^{-1})^T J_{12} \Lambda_{11}$.

$$\dot{V}_2 = -\tilde{x}_{12}^T \Lambda_{12} \Lambda_{11}^{-1} \tilde{x}_{12} \quad (28)$$

Now as previously choose λ_{11}^i and λ_{12}^i (the diagonal elements of the gain matrices Λ_{11} et Λ_{12}) large enough and $\Lambda_{13} = (M_1^{-1})^T J_{12} \Lambda_{11}$. Then convergence of (\hat{x}_{11} , \hat{x}_{21})

toward (x_{11}, x_{21}) is obtained and estimation errors on forces are bounded.

3.2 Observer for Suspensions dynamics Σ_2 :

We assume that the wheels are always in contact with the ground and note $\tilde{x}_{21} = \hat{x}_{21} - x_{21}$, $\tilde{x}_{22} = \hat{x}_{22} - x_{22}$ the state estimation error and $\tilde{F} = \hat{F} - F$ force estimation error. The proposed observer, for each wheel suspension, is:

$$\begin{cases} \dot{\tilde{x}}_{21} = \tilde{x}_{22} - \Lambda_{21} \text{sign}(\tilde{x}_{21}) \\ \dot{\tilde{x}}_{22} = \bar{M}_{33}^{-1}(J_3^T \tilde{F} - \bar{C}_{33} \tilde{x}_{22} - V_3 - \mu_2) - \Lambda_{22} \text{sign}(\tilde{x}_{21}) \\ \dot{\tilde{F}} = -P_2 \Lambda_{23} \text{sign}(\tilde{x}_{21}) \end{cases} \quad (29)$$

The observation error dynamics is given by:

$$\dot{\tilde{x}}_{21} = \tilde{x}_{22} - \Lambda_{21} \text{sign}(\tilde{x}_{21}) \quad (30)$$

$$\dot{\tilde{x}}_{22} = \bar{M}_{33}^{-1}(J_3^T \tilde{F} - \bar{C}_{33} \tilde{x}_{22}) - \Lambda_{22} \text{sign}(\tilde{x}_{21}) \quad (31)$$

$$\dot{\tilde{F}} = -P_2 \Lambda_{23} \text{sign}(\tilde{x}_{21}) \quad (32)$$

Like the previous case we choose $V_1 = \frac{1}{2} \tilde{x}_{21}^T \tilde{x}_{21}$ and show that \hat{x}_{12} converges to x_{12} in finite time t_{02} if we ensure that $\forall t > t_{02}$ that $|\tilde{x}_{22}| < \lambda_{21}^i$, (with $\Lambda_{21} = \text{diag}(\lambda_{21}^i)$, $i = 1..4$).

Then we deduce the reduced dynamics $\text{sign}_{\text{moy}}(\tilde{x}_{21}) = \Lambda_{21}^{-1} \tilde{x}_{22}$, if we replace this function by his expression in the equations (31), (32) we obtain:

$$\dot{\tilde{x}}_{22} = \bar{M}_{33}^{-1} J_3^T \tilde{F} - (\bar{M}_{33}^{-1} \bar{C}_{33} + \Lambda_{22} \Lambda_{21}^{-1}) \tilde{x}_{22} \quad (33)$$

$$\dot{\tilde{F}} = -P_2 \Lambda_{23} \Lambda_{21}^{-1} \tilde{x}_{22} \quad (34)$$

Let $V_2 = \frac{1}{2} \tilde{x}_{22}^T \bar{M}_{33} \tilde{x}_{22} + \frac{1}{2} \tilde{F}^T P_2^{-1} \tilde{F}$, its derivative \dot{V}_2 becomes, if we take $\Lambda_{23} = J_3 \Lambda_{12}$,

$$\dot{V}_2 = -\tilde{x}_{22}^T (\bar{C}_{33} + \bar{M}_{33} \Lambda_{22} \Lambda_{21}^{-1}) \tilde{x}_{22} \quad (35)$$

We can conclude as previously that if we choose λ_{21} and λ_{22} (the diagonal elements of the gain matrices Λ_{21} et Λ_{22}) large enough and $\Lambda_{23} = J_3 \Lambda_{21}$ then convergence of (\hat{x}_{21} , \hat{x}_{22}) toward (x_{21} , x_{22}) is obtained and estimation errors on forces \tilde{F} remains only bounded.

3.3 Observer for Wheels Dynamics Σ_3 :

By using the state space representation for the subsystem Σ_3 , the proposed observer, for each wheel, is as follows:

$$\begin{cases} \dot{\hat{x}}_{31} = \hat{x}_{32} - \Lambda_{31} \text{sign}(\hat{x}_{31} - x_{31}) \\ \dot{\hat{x}}_{32} = M_3^{-1} (\Gamma_{e45} - C_3 \hat{x}_{32} - V_{45} - \mu_3) - \Lambda_{32} \text{sign}(\tilde{x}_{31}) \\ \dot{\hat{F}} = -P_3 \Lambda_{33} \text{sign}(\hat{x}_{31} - x_{31}) \end{cases} \quad (36)$$

The vector Γ_{e45} is assumed known. This observer can be easily extended to estimate the torque by adding an equation defining the drive line producing the torque. Observation error dynamics is then:

$$\begin{cases} \dot{\tilde{x}}_{31} = \tilde{x}_{32} - \Lambda_{31} \text{sign}(\tilde{x}_{31}) \\ \dot{\tilde{x}}_{32} = -M_3^{-1} C_3 \tilde{x}_{32} - \Lambda_{32} \text{sign}(\tilde{x}_{31}) \\ \dot{\tilde{F}} = -P_3 \Lambda_{33} \text{sign}(\tilde{x}_{31}) \end{cases} \quad (37)$$

with $\tilde{x}_{31} = \hat{x}_{31} - x_{31}$, $\tilde{x}_{32} = \hat{x}_{32} - x_{32}$ the errors on estimations of states x_3 , and forces $\tilde{F} = \hat{F} - F$. We can prove the convergence in finite time (t_{03}) of states

estimates \hat{x}_{31} and bounded of forces estimation by using the Lyapunov functions:

$$V_1 = \frac{1}{2} \tilde{x}_{31} \tilde{x}_{31}^T \quad (38)$$

$$V_2 = -\frac{1}{2} \tilde{x}_{32} M_3 C_3^{-1} \tilde{x}_{32}^T \quad (39)$$

The derivatives of these functions are:

$$\dot{V}_1 = \tilde{x}_{31} (\tilde{x}_{32} - \Lambda_{31} \text{sign}(\tilde{x}_{31})) \quad (40)$$

$$\dot{V}_2 = -\tilde{x}_{32} C_3 M_3^{-1} (-M_3^{-1} C_3 \tilde{x}_{32} - \Lambda_{32} \text{sign}(\tilde{x}_{31})) \quad (41)$$

To guarantee that these derivatives are negative $\dot{V}_1 < 0$, $\dot{V}_2 < 0$ and consequently the convergence errors \tilde{x}_{31} , \tilde{x}_{32} goes to zero in finite time (t_{03}), we chose $\lambda_{31}^i = \text{diag}(\Lambda_{31})$, $\lambda_{32}^i = \text{diag}(\Lambda_{32})$ such as $\lambda_{31}^i > |\tilde{x}_{32}|$ and $\lambda_{32}^i > C_3^{-1} M_3 |\tilde{x}_{32}|$.

4. SIMULATION RESULTS

In this section, we give some simulation results got we the simulator previously developed by our staff (SimK106N) in order to test and validate the proposed observers and our approach of model splitting and developing partial state estimators. The system state evolution and forces are computed by use of a car simulation in Matlab - Simulink (fig.5). The model of the vehicle which allows

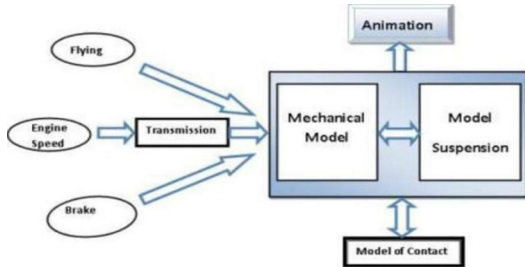


Fig. 5. Modular concept of the simulator

the resolution of the dynamics equation given by (1) is rewritten in following form:

$$\ddot{q} = M^{-1}(q)(\tau - C(q, \dot{q})\dot{q} - V(q, \dot{q}) - \eta_o(t, q, \dot{q}))$$

This has been computed with a symbolic toolbox (Maple) and embedded in the following programming structure to give our simulator called SimK106N. The used parameters and environment characteristics have been validated in a previous work in collaboration with the LCPC (ElHadri et al. [2000], M'sirdi et al. [2004], Rabhi et al. [2004]). The

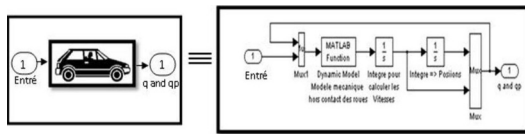


Fig. 6. Simulink block for the resolution of the equations of motion

simulation results presented by the figure (7), is obtained for a driving with sinusoidal steering command of 20 degrees amplitude. The results are good for the First Order Sliding Mode Observers. The model formulation has been done such the passivity property is preserved.

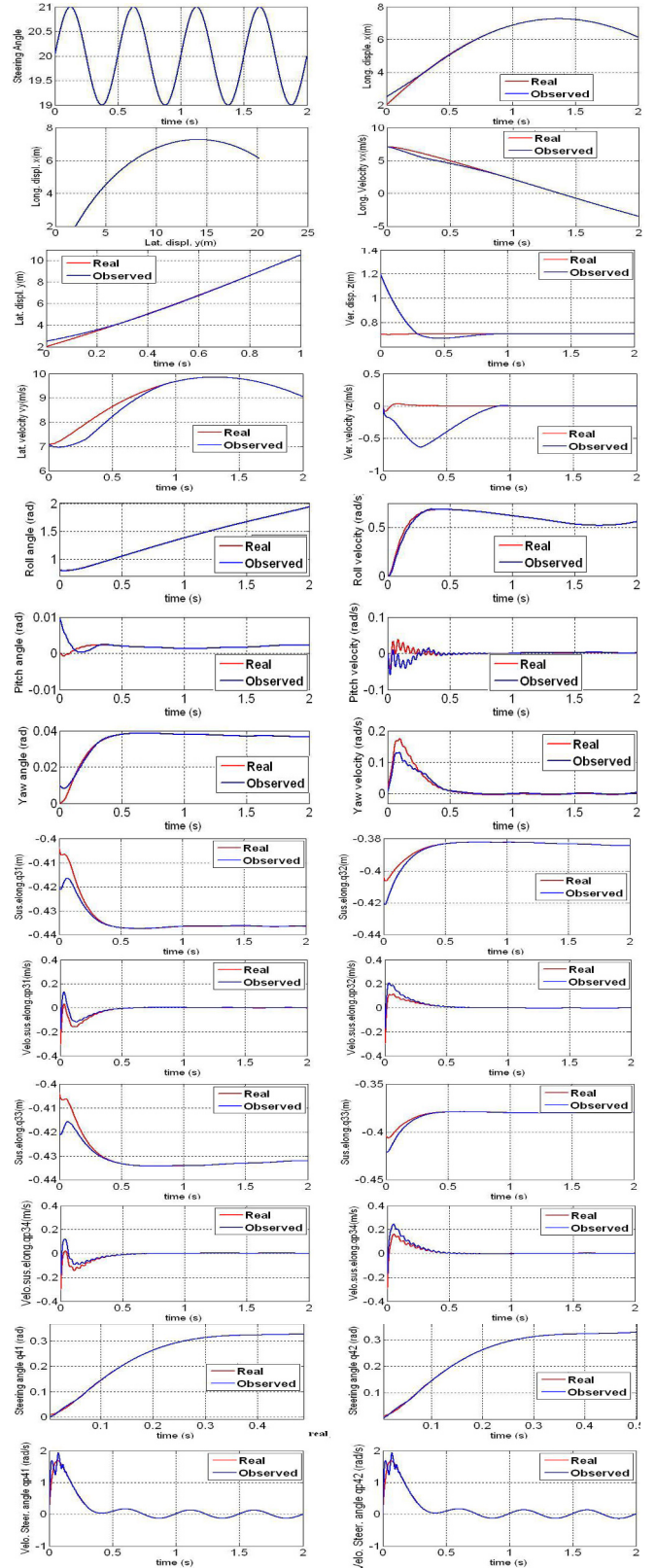


Fig. 7. Results of the First Order Sliding Mode observers

5. CONCLUSION

In this paper, we have proposed efficient and robust observers allowing to estimate states and unknown inputs (torques or forces). These observers obey to the first kind assuming that input forces and torques are constant or

slowly time varying ($\dot{F} \simeq 0$). The robustness of the sliding mode observer versus uncertainties on model parameters is an important feature. First Order Sliding Mode Observers have been developed and their performance evaluated. These observer are illustrated by simulation results to show effectiveness of their performance. These results validate the proposed observers and our approach of model splitting and developing partial state estimators.

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Appendix A. PARAMETERS OF THE MODELS

Definition of the matrices involved in the model.

$$\text{The inertia matrix: } M = \begin{bmatrix} \bar{M}_{11} & \bar{M}_{12} & \bar{M}_{13} & 0 & 0 \\ \bar{M}_{21} & \bar{M}_{22} & \bar{M}_{23} & \bar{M}_{24} & \bar{M}_{25} \\ \bar{M}_{31} & \bar{M}_{32} & \bar{M}_{33} & 0 & 0 \\ 0 & \bar{M}_{42} & 0 & \bar{M}_{44} & 0 \\ 0 & \bar{M}_{52} & 0 & 0 & \bar{M}_{55} \end{bmatrix}$$

$$\bar{M}_{11} = \begin{bmatrix} M_1^1 & 0 & 0 \\ 0 & M_2^2 & 0 \\ 0 & 0 & M_{33} \end{bmatrix} \quad \bar{M}_{12} = \bar{M}_{21}^T = \begin{bmatrix} M_1^4 & M_1^5 & M_1^6 \\ M_2^4 & M_2^5 & M_2^6 \\ 0 & M_3^5 & M_3^6 \end{bmatrix}$$

$$\bar{M}_{13} = \bar{M}_{31}^T = \begin{bmatrix} M_1^7 & M_1^8 & M_1^9 & M_1^{10} \\ M_2^7 & M_2^8 & M_2^9 & M_2^{10} \\ M_3^7 & M_3^8 & M_3^9 & M_3^{10} \end{bmatrix} \quad \bar{M}_{44} = \begin{bmatrix} M_{11}^{11} & 0 \\ 0 & M_{12}^{12} \end{bmatrix}$$

$$\bar{M}_{23} = \bar{M}_{32}^T = \begin{bmatrix} M_4^7 & M_4^8 & M_4^9 & M_4^{10} \\ M_5^7 & M_5^8 & M_5^9 & M_5^{10} \\ M_6^7 & M_6^8 & M_6^9 & M_6^{10} \end{bmatrix}$$

$$\bar{M}_{24} = \bar{M}_{42}^T = \begin{bmatrix} M_4^{11} & M_4^{12} \\ M_5^{11} & M_5^{12} \\ 0 & 0 \end{bmatrix} \quad \bar{M}_{33} = \begin{bmatrix} M_7^7 & 0 & 0 & 0 \\ 0 & M_8^8 & 0 & 0 \\ 0 & 0 & M_9^9 & 0 \\ 0 & 0 & 0 & M_{10}^{10} \end{bmatrix}$$

$$\bar{M}_{25} = \bar{M}_{52}^T = \begin{bmatrix} M_4^{13} & M_4^{14} & M_4^{15} & M_4^{16} \\ M_5^{13} & M_5^{14} & M_5^{15} & M_5^{16} \\ 0 & 0 & M_6^{15} & M_6^{16} \end{bmatrix}$$

$$\bar{M}_{22} = \begin{bmatrix} M_4^4 & M_4^5 & M_4^6 \\ M_5^4 & M_5^5 & M_5^6 \\ M_6^4 & M_6^5 & M_6^6 \end{bmatrix} \quad \bar{M}_{55} = \begin{bmatrix} M_{13}^{13} & 0 & 0 & 0 \\ 0 & M_{14}^{14} & 0 & 0 \\ 0 & 0 & M_{15}^{15} & 0 \\ 0 & 0 & 0 & M_{16}^{16} \end{bmatrix}$$

The coriolis and centrifugal matrix C :

$$C = \begin{bmatrix} 0 & \bar{C}_{12} & \bar{C}_{13} & 0 & 0 \\ 0 & \bar{C}_{22} & \bar{C}_{23} & \bar{C}_{24} & \bar{C}_{25} \\ 0 & \bar{C}_{32} & 0 & 0 & 0 \\ 0 & \bar{C}_{42} & 0 & 0 & \bar{C}_{45} \\ 0 & \bar{C}_{52} & 0 & \bar{C}_{54} & 0 \end{bmatrix}; \bar{C}_{12} = \begin{bmatrix} C_{14} & C_{15} & C_{16} \\ C_{24} & C_{25} & C_{26} \\ 0 & C_{35} & C_{36} \end{bmatrix};$$

$$\bar{C}_{13} = \begin{bmatrix} C_{17} & C_{18} & C_{19} & C_{110} \\ C_{27} & C_{28} & C_{29} & C_{210} \\ C_{37} & C_{38} & C_{39} & C_{310} \end{bmatrix}; \bar{C}_{22} = \begin{bmatrix} C_{44} & C_{45} & C_{46} \\ C_{54} & C_{55} & C_{56} \\ C_{64} & C_{65} & C_{66} \end{bmatrix};$$

$$\bar{C}_{24} = \bar{C}_{42}^T = \begin{bmatrix} C_{411} & C_{412} \\ C_{511} & C_{512} \\ C_{611} & C_{612} \end{bmatrix}; \bar{C}_{45} = \begin{bmatrix} 0 & 0 & C_{1115} & 0 \\ 0 & 0 & 0 & C_{1216} \end{bmatrix}$$

$$\bar{C}_{23} = \bar{C}_{32}^T = \begin{bmatrix} C_{47} & C_{48} & C_{49} & C_{410} \\ C_{57} & C_{58} & C_{59} & C_{510} \\ C_{67} & C_{68} & C_{69} & C_{610} \end{bmatrix};$$

$$\bar{C}_{25} = \bar{C}_{52}^T = \begin{bmatrix} C_{413} & C_{414} & C_{415} & C_{416} \\ C_{513} & C_{514} & C_{515} & C_{516} \\ C_{613} & C_{614} & C_{615} & C_{616} \end{bmatrix}$$

The Jacobian matrix: $J = [J_1^T J_2^T J_3^T 00]_{12 \times 16}^T$

$$J_1^T = \begin{bmatrix} J_1^1 & 0 & 0 & J_4^1 & 0 & 0 & J_7^1 & 0 & 0 & J_{10}^1 & 0 & 0 \\ 0 & J_2^2 & 0 & 0 & J_5^2 & 0 & 0 & J_8^2 & 0 & 0 & J_{11}^2 & 0 \\ 0 & 0 & J_3^3 & 0 & 0 & J_6^3 & 0 & 0 & J_9^3 & 0 & 0 & J_{12}^3 \end{bmatrix}$$

$$J_2^T = \begin{bmatrix} J_1^4 & J_2^4 & 0 & J_4^4 & J_5^4 & 0 & J_7^4 & J_8^4 & 0 & J_{10}^4 & J_{11}^4 & 0 \\ J_1^5 & J_2^5 & J_3^5 & J_4^5 & J_5^5 & J_6^5 & J_7^5 & J_8^5 & J_9^5 & J_{10}^5 & J_{11}^5 & J_{12}^5 \\ J_1^6 & J_2^6 & J_3^6 & J_4^6 & J_5^6 & J_6^6 & J_7^6 & J_8^6 & J_9^6 & J_{10}^6 & J_{11}^6 & J_{12}^6 \end{bmatrix}$$

$$J_3^T = \begin{bmatrix} J_1^7 & J_2^7 & J_3^7 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & J_4^8 & J_5^8 & J_6^8 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & J_7^9 & J_8^9 & J_9^9 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & J_{10}^{10} & J_{11}^{10} & J_{12}^{10} \end{bmatrix}$$