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Mixing Coefficient in Stably Stratified Flows

LAKSHMI KANTHA

Department of Aerospace Engineering Sciences, University of Colorado Boulder, Boulder, Colorado

HUBERT LUCE

Université de Toulon, Mediterranean Institute of Oceanography, UM 110, Marseille, France

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ABSTRACT

Turbulent mixing in the interior of the oceans is not as well understood as mixing in the oceanic boundary layers. Mixing in the generally stably stratified interior is primarily, although not exclusively, due to intermittent shear instabilities. Part of the energy extracted by the Reynolds stresses acting on the mean shear is expended in increasing the potential energy of the fluid column through a buoyancy flux, while most of it is dissipated. The mixing coefficient χ_m , the ratio of the buoyancy flux to the dissipation rate of turbulence kinetic energy ε , is an important parameter, since knowledge of χ_m enables turbulent diffusivities to be inferred. Theory indicates that χ_m must be a function of the gradient Richardson number. Yet, oceanic studies suggest that a value of around 0.2 for χ_m gives turbulent diffusivities that are in good agreement with those inferred from tracer studies. Studies by scientists working with atmospheric radars tend to reinforce these findings but are seldom referenced in oceanographic literature. The goal of this paper is to bring together oceanographic, atmospheric, and laboratory observations related to χ_m and to report on the values deduced from in situ data collected in the lower troposphere by unmanned aerial vehicles, equipped with turbulence sensors and flown in the vicinity of the Middle and Upper Atmosphere (MU) radar in Japan. These observations are consistent with past studies in the oceans, in that a value of around 0.16 for χ_m yields good agreement between ε derived from turbulent temperature fluctuations using this value and ε obtained directly from turbulence velocity fluctuations.

1. Introduction

Apart from the well-mixed turbulent layers adjacent to the air-sea interface and the ground and above the ocean bottom, for the most part, the fluid columns in both the oceans and the atmosphere are stably stratified. As such, turbulent mixing in the interior of the oceans and in the free atmosphere above the atmospheric boundary layer (ABL) occurs under the influence of stable gravitational stratification. The principal mechanism is thought to be flow instability induced by the vertical shear of the horizontal velocity (e.g., Fukao et al. 2011). The Miles–Howard theorem (Miles 1961; Howard 1961) assures flow stability in a two-dimensional, parallel, inviscid shear flow, as long as the gradient Richardson number Ri > 0.25 everywhere in the flow. When the local gradient Richardson number falls below a value of approximately 0.25 (e.g., Abarbanel et al. 1984), the flow becomes unstable and can give raise to Kelvin– Helmholtz billows, which mix the fluid, weaken the

shear, and restore stability. However, the precise value

When the fluid is stably stratified, part of the energy input to creating turbulence goes to increase the potential energy of the fluid column through a vertical buoyancy flux. The rest is dissipated. The ratio of the

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of the critical Richardson number at which instability ensues is affected by viscosity, by diffusivity (Thorpe et al. 2013), and possibly by background ambient turbulence (Li et al. 2015). Shear instabilities can also be triggered by gravity waves propagating into the interior, which are the principal source of mixing [e.g., the recent review by Tsuda (2014)] in the middle and upper atmosphere (10–100 km). However, midlevel cloud-base turbulence (Kudo 2013; Kudo et al. 2015) and double-diffusive processes (e.g., Kantha et al. 2011) are exceptions to this rule in the moist troposphere and the oceans, respectively. Both can drive mixing without the need for any vertical shear.

Corresponding author: Lakshmi Kantha, kantha@colorado.edu

buoyancy flux to the dissipation rate of turbulence kinetic energy (TKE) is known as the mixing coefficient χ_m . It is difficult to measure the buoyancy flux directly, but knowing the value of χ_m enables the buoyancy flux to be estimated, provided the TKE dissipation rate (per unit mass) ε is known. The TKE dissipation rate can be readily measured in the ocean using microstructure profilers, but a similar probe has not been available in the atmosphere. As such, there has been more interest among oceanographers than among atmospheric scientists in estimating the mixing coefficient (but see below). While there have been some studies of the mixing coefficient (equivalently, the flux Richardson number R_f in the atmosphere in the past (e.g., Delage et al. 1997), the availability of inexpensive, autonomous unmanned aerial vehicle (UAV) technology in recent years has enabled in situ measurements of turbulence parameters and, therefore, routine estimation of the mixing coefficient in the atmosphere.

There have been many measurements of the mixing coefficient in the ocean (e.g., Peters et al. 1995; St. Laurent and Schmitt 1999; Arneborg 2002; Mack and Schoeberlein 2004; Holleman et al. 2016). Most observations find its value lies between 0.1 and 0.3, for the most part, although the scatter is very large. Gregg et al. (2018) have published a comprehensive and authoritative survey recently, and there is no need to repeat their findings here. Instead, the reader is referred to their study and the comprehensive list of references cited therein. While turbulence theory requires the mixing coefficient to be a function of the strength of stable stratification as indicated by the gradient Richardson number Ri, tracer studies on turbulent diffusion in the upper ocean are consistent with the mixing coefficient value of about 0.2 (e.g., Ledwell et al. 1998, 2000, 2004; Gregg et al. 2018). There are other studies reviewed by Peltier and Caulfield (2003) that also offer "compelling" evidence that while the value of the mixing coefficient can be very high during the initial stages of Kelvin-Helmholtz shear instability (but the degree of mixing can be small), in later stages when the flow truly undergoes transition to turbulence, intense mixing ensues, and the mixing coefficient becomes approximately constant at around 0.2. This result is puzzling. Does it mean that, for some reason, the most likely value of the mixing coefficient in the upper ocean is around 0.2? If so, why? These questions need to be addressed. Meanwhile, Gregg et al. (2018) recommend that oceanographers continue using this constant value for the mixing coefficient until related issues can be resolved by further research and gathering observational data in the interior of the oceans.

Turbulent mixing has also been studied in the laboratory (e.g., Thorpe 1973; McEwan 1983; Rohr and Van Atta 1987; Ivey and Imberger 1991; Taylor 1992). Kantha and Carniel (2009) compare their turbulence model with available laboratory data (from Ohya 2001; Strang and Fernando 2001; Rehmann and Koseff 2004) on the Ri dependence of R_f (and therefore indirectly χ_m). As for numerical simulations of mixing, even with highperformance computers, the salient turbulence Reynolds numbers achievable at present are far less than the values in the oceans and the atmosphere, and this is a major problem in extrapolating those results to realistic Reynolds numbers. For a discussion of laboratory observations and numerical simulations (e.g., Zilitinkevich 2007, 2008), see the nice summary by Gregg et al. (2018).

There have also been some studies of the turbulent mixing coefficient in stably stratified flows by atmospheric scientists, starting with Lilly et al. (1974), who suggested a value of 0.33 corresponding to the upper limit on the flux Richardson number of 0.25. However, in situ measurements in the atmosphere require specially equipped aircraft and hence were expensive and scarce (e.g., Lilly 1983). This situation has changed, but only recently, by the ready availability of inexpensive UAVs (e.g., Lawrence and Balsley 2013; Kantha et al. 2017).

On the other hand, researchers working with atmospheric radars are very much interested in the value of a particular parameter γ , which is inversely proportional to the mixing coefficient χ_m (see section 2), because of its importance in deducing atmospheric parameters from radar backscatter data. Alisse and Sidi (2000) and Alisse et al. (2000) determined the value for the mixing coefficient, from high-resolution in situ measurements in the lower stratosphere to the upper troposphere, to be 0.12 ± 0.06 . From high-resolution radar measurements in the lower troposphere, Dole et al. (2001) found it to be 0.2 ± 0.1 , whereas high-resolution radar measurements of Wilson et al. (2005) found a median value of 0.16. These observations tend to reinforce the findings of oceanographers. However, a nice review by Hocking (1999) points out that the Ri dependence of γ and hence the mixing coefficient was mostly ignored in the radar literature (e.g., VanZandt et al. 1978, 1981; Gage et al. 1980; Hocking 1985; Thrane et al. 1985, 1987; Lübken 1992; Lübken et al. 1987; Blix et al. 1990), although some studies such as Ottersten (1969), Crane (1980), Gossard and Strauch (1983), Gossard (1990), Gossard et al. (1982, 1984, 1985), Hocking (1992), Blix (1993), Hocking (1996), Hocking and Mu (1997), and Hocking (1999) have acknowledged the Ri dependence of the parameter γ and hence χ_m . In any case, studies by atmospheric radar scientists have seldom been referenced in oceanic studies, although radar scientists often reference oceanic studies (e.g., Hocking 1999).

From all of these past studies, it is fair to conclude that even though scatter is large, the value of the mixing coefficient in both the oceans and the atmosphere appears to lie mostly between values of 0.1 and 0.3. However, more often than not, the gradient Richardson number Ri associated with the observed values of the mixing coefficient is not measured and hence remains unknown [see the review by Gregg et al. (2018)]. Consequently, most of these studies cannot shed light on the issue of Ri dependence of χ_m or why a value of around 0.2 yields acceptable diffusivities. It is our intent to present in situ data in the lower troposphere collected at the Middle and Upper Atmosphere (MU) radar observatory in Shigaraki, Japan, during a 2016 field campaign to supplement past studies in the oceans and the laboratory and to provide additional data, which are from the atmosphere and hence independent of oceanic studies. We found that the mixing coefficient in the lower troposphere under stably stratified conditions has a lognormal distribution with the peak at a value of about 0.16. This value is not equal to but is within 80% of the abovementioned value of 0.2, suggesting that perhaps in both the oceans and the atmosphere, the most likely value for the mixing coefficient is around 0.16-0.20. We also elaborate on the Ri dependence of χ_m and speculate on why assuming a constant χ_m value of somewhere between 0.16 and 0.20 might be a good approximation in the interiors of the oceans and the atmosphere under stably stratified conditions. In section 2, we provide a brief review of the governing equations for potential use by oceanographers unfamiliar with radar terminology and to prevent confusion related to disparate notations used in different fields. Section 3 presents observations, and section 4 provides concluding remarks.

2. Governing equations

We start with the equation for the rate of change of TKE:

$$d(\text{TKE})/dt = P_s + F_b - \varepsilon, \qquad (1)$$

where

$$P_{S} = \left(-\overline{uw}\frac{\partial U}{\partial z} - \overline{vw}\frac{\partial V}{\partial z}\right)$$
(2)

is the rate of TKE production by Reynolds stresses acting on the mean vertical shear,

$$F_b = \frac{g}{\Theta} \overline{w\theta} \tag{3}$$

is the buoyancy flux, and ε is the dissipation rate. Here, U and V are velocity components in the x and y directions and Θ is the mean potential temperature. For turbulence in equilibrium,

$$P_{g} + F_{b} - \varepsilon = \left(-\overline{uw} \frac{\partial U}{\partial z} - \overline{vw} \frac{\partial V}{\partial z} \right) + \frac{g}{\Theta} \overline{w\theta} - \varepsilon = 0.$$
(4)

Shear production is always positive and hence a source of TKE. The buoyancy flux is positive and hence a source of TKE during convection, but under stable stratification it is negative and is hence a sink of TKE. Dissipation is always a sink. We can write

$$-\overline{uw} = K_M \frac{\partial U}{\partial z}, \quad -\overline{vw} = K_M \frac{\partial V}{\partial z}, \quad \text{and} \quad -\overline{w\theta} = K_\theta \frac{\partial \Theta}{\partial z},$$
(5)

where K_M and K_{θ} are coefficients of mixing of momentum and heat, respectively, so that

$$F_b = -K_\theta N^2. \tag{6}$$

Equation (1) can also be written as

$$K_M S^2 - K_\theta N^2 - \varepsilon = 0, \qquad (7)$$

with

$$S^{2} = \left(\frac{\partial U}{\partial z}\right)^{2} + \left(\frac{\partial V}{\partial z}\right)^{2}$$
(8)

being the square of the shear frequency S and

$$N^2 = \frac{g}{\Theta} \left(\frac{\partial \Theta}{\partial z} \right) \tag{9}$$

being the square of the buoyancy frequency N. The ratio

$$\mathrm{Ri} = N^2 / S^2 \tag{10}$$

is the gradient Richardson number and is indicative of the degree of static stability of the fluid column. For Ri > 0, the column is stably stratified; for Ri < 0, it is unstably stratified. The ratio of the buoyancy flux to shear production is the flux Richardson number:

$$R_f = -F_b/P_s. \tag{11}$$

By using Eq. (11) to replace P_S in Eq. (4),

$$-F_b = \left(\frac{R_f}{1 - R_f}\right)\varepsilon = \chi_m \varepsilon, \qquad (12)$$

where

$$\chi_m = -\frac{F_b}{\varepsilon} = \frac{R_f}{1 - R_f} \tag{13}$$

is the ratio of the absolute value of the buoyancy flux to the dissipation rate. The term χ_m is the so-called mixing coefficient, even though it is widely known as the mixing efficiency in oceanic turbulence literature (the ratio of buoyancy flux to shear production R_f is the *true* mixing efficiency). Because the flux Richardson number R_f is a function of the gradient Richardson number Ri, the mixing coefficient χ_m must also be a function of Ri.

The buoyancy flux increases the potential energy of the fluid column; therefore, how much of the energy input into turbulence goes to increase the potential energy has always been of interest to oceanographers. However, shear production and buoyancy flux are hard to measure both in the oceans and in the atmosphere, whereas measurement of ε in the ocean is relatively straightforward using microstructure profilers. Therefore, a quantity of great interest to oceanographers is the mixing coefficient χ_m .

Microstructure profilers are free-falling, torpedoshaped objects deployed from stationary ships and carry airfoil probes in the nose whose lateral deflections can be readily measured using piezoelectric sensors. Using a series of assumptions, especially on the shape of the turbulence shear spectrum, these measurements can be translated into estimates of ε (e.g., Carniel et al. 2012). The profilers also carry sensors to measure temperature, salinity, and pressure. High-frequency-response thermistors enable the dissipation rate χ_T of temperature variance also to be inferred. These profilers have been developed and refined over the past few decades and are now routinely deployed in the global oceans to measure TKE dissipation rates.

In turbulence studies, it is traditional to define structure functions for various quantities. For potential temperature more appropriate to atmospheric flows, the structure function is

$$D_{\theta}(r) = \langle [\Theta(x+r) - \Theta(x)]^2 \rangle.$$
(14)

In the inertial subrange of the turbulence spectrum,

$$D_{\theta}(r) = C_{\theta}^2 r^{2/3}, \qquad (15)$$

where C_{θ}^2 is the structure-function parameter for potential temperature and is a measure of the potential energy fluctuations.

The rate of change of potential temperature variance $\overline{\theta^2}$ is given by

$$\frac{d}{dt}(\overline{\theta^2}) = 2(P_\theta - \chi_\theta), \qquad (16)$$

where

$$P_{\theta} = -\overline{w\theta}(d\Theta/dz) \tag{17}$$

is the rate of production of potential temperature variance and χ_{θ} is its dissipation rate. For turbulence in equilibrium,

$$-\overline{w\theta}(\partial\Theta/\partial z) = \chi_{\theta} \tag{18}$$

so that

$$\chi_{\theta} = K_{\theta} (d\Theta/dz)^2.$$
⁽¹⁹⁾

From Eqs. (6) and (13),

$$K_{\theta} = \chi_m \varepsilon / N^2, \qquad (20)$$

and therefore the mixing coefficient is

$$\chi_m = \frac{\chi_\theta N^2}{\varepsilon (d\Theta/dz)^2}.$$
 (21)

Because all of the quantities on the rhs of Eq. (19) can be measured by microstructure profilers, the mixing coefficient is readily estimated in the oceans. From Eqs. (9) and (20),

$$\chi_{\theta} = K_{\theta} \left(\frac{\Theta N^2}{g}\right)^2.$$
 (22)

Now, the one-dimensional potential temperature spectrum in the inertial subrange can be written in terms of either χ_{θ} or C_{θ}^2 as

$$S_{\theta}(k) = \beta \varepsilon^{-1/3} \chi_{\theta} k^{-5/3} = \alpha C_{\theta}^2 k^{-5/3}, \qquad (23)$$

where $\alpha \approx 0.25$ and $\beta \approx 0.75$ –1.0, although a value of 0.8 is more commonly used. From Eq. (23), it is easy to see that

$$C_{\theta}^{2} = B_{\theta} \varepsilon^{-1/3} \chi_{\theta}; \quad B_{\theta} = \beta / \alpha \,. \tag{24}$$

By using Eq. (24) to replace χ_{θ} by C_{θ}^2 in Eq. (22),

$$K_{\theta} \left(\frac{\Theta N^2}{g}\right)^2 = \left(\frac{C_{\theta}^2}{B_{\theta}}\right) \varepsilon^{1/3}.$$
 (25)

By using Eq. (20) then to substitute for K_{θ} ,

$$\varepsilon = \left(\frac{C_{\theta}^2 g^2}{B_{\theta} \chi_m \Theta^2 N^2}\right)^{3/2} = \left(\frac{\gamma C_{\theta}^2 g^2}{\Theta^2 N^2}\right)^{3/2}, \qquad (26)$$

where

$$\gamma = \left(B_{\theta}\chi_m\right)^{-1} \tag{27}$$

is the parameter widely used in radar literature (e.g., Hocking 1999). Therefore, measured values of C_{θ}^2 can

be used to estimate the TKE dissipation rate ε from Eq. (26), or equivalently, if ε and C_{θ}^2 are known, γ and the mixing coefficient χ_m can be determined.

The flux Richardson number [Eq. (11)] can also be written as

$$R_{f} = \frac{K_{\theta}}{K_{M}} \left(\frac{N^{2}}{S^{2}} \right) = \operatorname{Ri} \left(\frac{K_{\theta}}{K_{M}} \right) = \frac{\operatorname{Ri}}{\operatorname{Pr}_{t}}, \quad (28)$$

where

$$\Pr_t = K_M / K_\theta \tag{29}$$

is the turbulent Prandtl number, so that γ can also be written as

$$\gamma = \frac{(\Pr_t - Ri)}{B_a Ri}.$$
 (30)

By using the identity

$$\Pr_t = \operatorname{Ri}/R_f \tag{31}$$

in Eq. (30),

$$\gamma = \frac{1}{B_{\theta}} \left(\frac{1 - R_f}{R_f} \right) = \frac{1}{B_{\theta} \chi_m}.$$
 (32)

Thus γ is inversely proportional to the mixing coefficient so that by using Eq. (20) χ_m , and vice versa:

$$\chi_m = (B_\theta \gamma)^{-1}, \qquad (33)$$

with B_{θ} having values between 3 and 4, with the most commonly used value being 3.2 (e.g., Gossard et al. 1982, 1984). Note that

$$R_f = \frac{\chi_m}{1 + \chi_m}.$$
 (34)

Using second-moment closure of turbulence, Kantha (2003) and Kantha and Carniel (2009) have obtained R_f as a function of Ri in stably stratified flows. These results can be approximated very well (see Figs. 6 and 7 below) by the empirical expression

$$R_{f} = R_{f}^{\max} \left[1 - \exp\left(-\frac{\mathrm{Ri}}{R_{f}^{\mathrm{max}} \mathrm{Pr}_{t}^{0}}\right) \right], \qquad (35)$$

where R_f^{\max} is the maximum flux Richardson number in the limit $Ri \rightarrow \infty$, and Pr_t^0 is the Prandtl number at Ri =0 (neutrally stratified flows). Equations (33)–(35) can then be used to compute χ_m and hence γ from measured values of Ri. As a corollary, Ri can be determined

(if unknown) from Eqs. (33)-(35) from values of γ inferred from simultaneous measurements of ε and C_{θ}^2 using Eq. (24). By using Eqs. (31) and (35), Pr_t can be related to Ri by the equation

$$\frac{1}{\Pr_{t}} = \frac{R_{f}^{\max}}{\operatorname{Ri}} \left[1 - \exp\left(-\frac{\operatorname{Ri}}{R_{f}^{\max}\operatorname{Pr}_{t}^{0}}\right) \right].$$
(36)

In situ measurements of temperature are often used in many studies, and the structure-function parameter of temperature in the inertial subrange is then defined as

$$D_T(r) = C_T^2 r^{2/3}, (37)$$

where

$$D_T(r) = \langle \left[T(x+r) - T(x)\right]^2 \rangle.$$
(38)

Also, from Tatarskii (1961),

$$\chi_T = K_T \left(\frac{dT}{dz} + \Gamma_a\right)^2 = K_T \left(\frac{T}{\Theta} \frac{d\Theta}{dz}\right)^2$$
(39)

and

$$C_T^2 = B_T \varepsilon^{-1/3} \chi_T, \qquad (40)$$

$$\varepsilon = \left\{ \left(\frac{K_{\theta}}{K_T} \right) \left(\frac{B_{\theta}}{B_T} \right) \left[\frac{C_T^2 N^2 \Theta^2}{B_{\theta} \chi_m T^2 (d\Theta/dz)^2} \right] \right\}^{3/2} \\ = \left(\frac{\gamma C_T^2 g^2}{T^2 N^2} \right)^{3/2}.$$
(41)

Radar signals are backscattered from refractive index fluctuations in the atmosphere, and so it is common to use turbulence parameters based on fluctuations in the refractive index n, assuming inertial subrange:

$$D_n(r) = C_n^2 r^{2/3}, (42)$$

where

and

$$D_n(r) = \langle [n(x+r) - n(x)]^2 \rangle, \qquad (43)$$

$$\chi_n = K_n (dn/dz)^2 = K_n M^2,$$
 (44)

$$C_n^2 = B_n \varepsilon^{-1/3} \chi_n \tag{45}$$

so that, by using (20),

$$\varepsilon = \left\{ \left(\frac{K_{\theta}}{K_n}\right) \left(\frac{B_{\theta}}{B_n}\right) \left[\frac{C_n^2 N^2}{B_{\theta} \chi_m (dn/dz)^2}\right] \right\}^{3/2} = \left(\frac{\gamma C_n^2 N^2}{M^2}\right)^{3/2}.$$
(46)

Equations (46) and (41) or Eq. (26) can be used to estimate γ and hence χ_m .

Although this study is focused on stably stratified flows, convective turbulence is also of great interest in both the atmosphere and the oceans, for which Eqs. (2) and (16) yield

$$\chi_m = -1 \tag{47}$$

since shear production $P_S = 0$. Substituting for χ_m in Eq. (41), we get

$$\varepsilon = \left[\frac{C_T^2 g^2}{B_\theta T^2 (-N^2)}\right]^{3/2}.$$
(48)

Note that $N^2 < 0$ in a convective layer.

3. ShUREX 2016 observations

The Shigaraki MU radar observatory (Fukao et al. 1985a,b), run by the Research Institute for Sustainable Humanosphere of the Kyoto University in Japan, is located in Shigaraki (34.854061°N, 136.105606°E) at a height of 378 m above sea level (MSL). It consists of a variety of instruments for measuring and monitoring the atmospheric column, the principal one being the 103-m-diameter, 46.5-MHz MU radar. During the Shigaraki UAV-Radar Experiment (ShUREX) campaigns at the Shigaraki observatory, turbulence sensors deployed on DataHawk UAVs, which were developed at the University of Colorado by D. Lawrence (Lawrence and Balsley 2013), were flown in the immediate vicinity of the MU radar to obtain in situ measurements of turbulence parameters near the radar (see Kantha et al. 2017). A high-frequency-response Pitot tube system was used to measure velocity fluctuations, from which the TKE spectrum was deduced and used to estimate the TKE dissipation rate ε . Temperature fluctuations were also measured using a high-frequency-response (800 Hz) cold-wire sensor and were used to estimate C_T^2 . Three ShUREX campaigns were conducted at the observatory during the spring-summer seasons of 2015, 2016, and 2017. A principal goal of these campaigns was to obtain in situ measurements of ε and C_T^2 in the lower troposphere, guided and supplemented by radar observations so that interesting atmospheric structures could be identified by the radar in near-real time and probed by the UAV. See Kantha et al. (2017) for a more detailed description of ShUREX campaigns, the sensors deployed, and analysis of turbulence data. [See Kantha et al. (2018, manuscript submitted to *Earth Planets Space*) and Luce et al. (2018, manuscript submitted to *Earth Planets Space*) for details on extracting turbulence properties from radar backscattered signal.] Hocking et al. (2016) summarize very well the existing state of the art in the use of atmospheric radars for measurements of 3D velocity field and turbulence in the atmospheric column above the radar.

All of the UAV flights were undertaken from a field roughly 1km southeast of the MU radar. For most measurements, the UAV ascended and descended over the field in a spiral path of roughly 100-m diameter at a vertical velocity of about $2 \,\mathrm{m \, s^{-1}}$. We will restrict ourselves to the 2016 data for this study. A total of 45 flights were conducted between 21 May and 13 June 2016, of which roughly 16 flights (flights 5, 8, 9, 15, 17, 18, 21, 22, 28, 30, 31, 32, 37, 38, 40, and 41) yielded useful scientific data. Of these, flights 17, 18, 21, and 32 were primarily in the convective boundary layer (CBL) and therefore were not included in this study. The remainder of the flights probed mostly a stably stratified atmospheric column above a shallow CBL, and once again the data inside the CBL and any convective and cloudy regions in the atmospheric column were excluded from the study.

The stable atmospheric column above the CBL consisted mostly of "sheets and layers" types of structures, although at times, there were imbedded convective structures below the cloud base created by evaporation of ice particles in the dry air layer below the cloud base. Data in these convective regions were discarded. For brevity, we will not describe the data analysis procedures here but instead refer readers to H. Luce (2018, unpublished manuscript).

The sheets-and-layers structures (apparently turbulent layers separated by thin sheetlike regions) were produced by humidity gradients in the presence of water vapor in the atmosphere. The backscattered signal of the VHF radar is especially sensitive to humidity gradients and highlights even small humidity gradients, which appear then as dark sheets (see Fig. 1). As such, these sheets-and-layers structures seen above the CBL in the moist troposphere may not be dynamically significant at all. Turbulence above the CBL is still generated predominantly by shear, as measurements show. Most important, these sheetlike structures are not the same as those seen sometimes in the oceanic thermocline, where they do highlight strong density gradients of dynamical significance.

Figure 1 shows a typical radar image, obtained during UAV flight 5 on 30 May 2016. The fainter line shows the UAV track, and the dark line below it shows the altitude above sea level of the UAV. Near-real-time radar

Capon power (0°,0°) (FLT05)



FIG. 1. MU radar image during UAV flight 5 on 30 May 2016. The dark line shows the altitude of the UAV, and the fainter line immediately above it shows the radar track of the UAV (i.e., range) ascending and descending in a spiral pattern.

images like this were very useful for understanding what exactly the UAV was probing and for directing it, if need be, to probe interesting nearby atmospheric structures. The radar can detect structures only above 1.3 km MSL, and, as can be seen, the ABL height was less than 1.3 km during UAV ascent but increased to about 1.5 km MSL during descent. As such, the UAV measured stably stratified regions above roughly 1.5-km MSL altitude.

The left-hand panels of Figs. 2a and 2b show the vertical profiles of ε (thick blue line) and C_T^2 (thick cyan line) during ascent and descent phases of flight 5, respectively. The thin black line shows measured N^2 . The extent of the CBL, where properties are relatively more uniform, is shown by a gray rectangle extending from 0 to 1200 m in Fig. 2a and to 1500 m in Fig. 2b, consistent with the radar image in Fig. 1. Since the CBL extends to only about 1200 m MSL during ascent, it cannot be seen in Fig. 1. The atmosphere above the CBL consists of the so-called sheets and layers. The center panels compare ε measured directly by the UAV with ε derived from C_T^2 [using Eq. (41)] using measured values of N^2 (thin black line) and assuming a constant value of 1.95 for γ (equivalent to χ_m of 0.16). The two track each other very well. The right-hand panels show the same quantities but using a standard value for N^2 $(1.47 \times 10^{-4} \text{ s}^{-2})$ in the troposphere in Eq. (41). The red curve indicates that there is a good agreement between measured ε (thick blue line) and that derived from C_T^2 (thick red line) in the CBL, if N^2 is taken as 0.4×10^{-4} . However, since an χ_m value of 0.16 is used in Eq. (41) but $\chi_m = -1$ in the CBL, this is equivalent to $N^2 \approx -6.4 \times$ 10^{-6} s⁻¹ in the CBL [Eq. (48)].

Figure 3 shows a histogram of the mixing coefficient χ_m obtained from UAV measurements of ε and C_T^2 [using Eqs. (33) and (41)], plotted in both log and linear scales for all flights. A few data points that fall above the absolute theoretical upper bound of 1.0 have been omitted. The

theoretical upper bound of $\frac{1}{3}$ from turbulence theory (e.g., Kantha and Carniel 2009) is also shown. The extended vertical lines show that the peak of the distribution occurs at a value of about 0.16 (it is also the median value), close to the value of 0.2 cited in oceanographic literature.

Figure 4 shows a scatterplot of ε measured directly by the UAV against those derived from C_T^2 , assuming a constant value of 1.95 for γ , equivalent to mixing coefficient χ_m of 0.16. There is a remarkably tight correlation between the two that appears to justify the use of a constant value of 0.16 for the mixing coefficient in turbulence studies.

Technical difficulties have hindered accurate determination of wind velocities (and hence Ri) directly from UAV measurements. The radar itself can infer Ri only at scales of 150 m and above. Therefore, we use the value of Ri determined from radiosondes released during the flights. Only flights 8, 15, 28, and 41 are considered, since radiosondes released during the flight were available and stably stratified conditions prevailed over the CBL. Table 1 shows conditions for these flights.

Note that the UAV flights were made 1 km southwest of the radar and radiosondes were released at the radar site and drifted away from both the radar and the UAV. The ascent rates of the UAV and the radiosonde were not the same. Consequently, there could be a vertical shift in altitude of properties measured by the radiosonde relative to the UAV. Therefore, Ri values were computed from radiosonde data as a function of altitude by locally shifting the radiosonde N^2 profiles vertically until they matched the N^2 profiles measured by the UAV. One can therefore expect some scatter in the results, since the radiosonde and the UAV are not measuring the same volume in the atmospheric column. Measurements at Shigaraki have shown a remarkable degree of horizontal homogeneity (except for small vertical shifts, presumably due to wave motions) in properties over scales of 5-10 km



FIG. 2. Vertical profiles of various quantities during the (a) ascent and (b) descent phases of UAV flight 5: (left) profiles of measured values of ε (thick blue line), C_T^2 (thick cyan line), and N^2 (thin black line); (center) measured ε (thick blue line) and ε derived from C_T^2 (thick black line) using measured values of N^2 (thin black line) and assuming a constant value of 1.95 for γ (equivalently χ_m of 0.16); (right) measured ε (thick blue line) and ε derived from C_T^2 (thick black and red lines) using constant values for N^2 , assuming constant value of 1.95 for γ (equivalently χ_m of 0.16).



FIG. 2. (Continued)



FIG. 3. Histogram of the mixing coefficients χ_m deduced from UAV observations of ε and C_T^2 . From left to right, the vertical lines are for $\chi_m = 0.16, 0.2, 0.33$, and 1.0.

(Luce et al. 2018). When Luce et al. (2018) compared radar-measured values with radiosonde-measured values for parameters such as N^2 and M^2 (indicative of the gradients of density and humidity), there was remarkable agreement. It appears that the radiosonde and the radar are measuring the same features and, by extension then, the UAV and radiosonde are measuring the same parameters with a slight delay. The estimates of Ri profiles by the radar and the radiosonde also showed remarkable agreement at all altitudes. Therefore, all three instruments detected the same prominent temperature and humidity gradients, down to decameter scales in stratified conditions. These gradients extended horizontally over a few kilometers at least and persisted for hours without significant changes [see Luce et al. (2018) and Luce et al. (2018, manuscript submitted to Earth Planets Space) for details and measurement errors; see also Balsley et al. (2010) for radiosonde measurements of velocity and Ri.

Measurements of ε and the local buoyancy frequency N enable the so-called buoyancy Reynolds number

$$\operatorname{Re}_{h} = \varepsilon / (\nu N^{2}) \tag{49}$$

to be extracted from ShUREX observations; Re_b is also called turbulence activity by oceanographers (e.g., Gregg et al. 2018; Gibson 1980), who use it as a measure of the strength of the turbulent mixing. The Re_b can also be written as

$$\operatorname{Re}_{b} = \left[\frac{(\varepsilon/N^{3})^{1/2}}{(\nu^{3}/\varepsilon)^{1/4}}\right]^{4/3} = \left(\frac{L_{O}}{L_{K}}\right)^{4/3} \approx 13.9 \left(\frac{L_{\text{outer}}}{L_{\text{inner}}}\right)^{4/3},$$
(50)

where L_O is the Ozmidov scale, which denotes the outer scale of turbulence L_{outer} , and L_K denotes the Kolmogoroff viscous scale, which is proportional to the inner scale of turbulence L_{inner} [~(7.2–12.4) L_K]. The inner and outer scales delimit the Kolmogoroff inertial subrange (ISR) of turbulence kinetic energy spectrum, where turbulence is expected to be isotropic. The ratio of the two scales,

$$R = L_{\rm outer} / L_{\rm inner}, \tag{51}$$

is a measure of how well developed turbulence is. The Re_b is related to R by

$$\operatorname{Re}_{b} = 13.9R^{4/3}$$
. (52)



FIG. 4. Scatterplot of ε derived from C_T^2 measurements, assuming a γ value of 1.95, against those measured directly by the Pitot sensor.

Flight No.	Date	Launch time for UAV (LT)	Launch time for radiosonde (LT)	Flight duration for UAV (min)	Max. alt for UAV (km)
8	28 May	1110:37	1205:00	81	4.0
15	30 May	1434:43	1458:00	80	4.0
28	8 Jun	0941:28	1013:00	99	4.0
41	13 Jun	1410:10	1420:54	90	4.5

TABLE 1. A list of UAV flights during which radiosondes were released from the MU radar site. Data from these flights are used in the study.

Therefore, Re_b is, in strict terms, not the turbulence Reynolds number but more appropriately is a measure of the broadness of the ISR. For turbulence to be well established, *R* must have a value of at least 2, and therefore Re_b must be above 35. Oceanographers dealing with doublediffusive mixing often use the value of 25 as the upper limit of that type of mixing. For R = 10 (one decade of ISR in the turbulence spectrum), $\text{Re}_b \approx 300$; for R = 1000 (three decades), $\text{Re}_b \approx 1.4 \times 10^5$. Typical observations of Re_b in the interior of the oceans (see Gregg et al. 2018) show that the ISR extends to between one and three decades in the TKE spectrum (Peters et al. 1995, their Fig. 10).

Figure 5 shows Re_b plotted against Ri from ShUREX 2016 observations. The values lie mostly between 10^2 and 10^6 . The upper value corresponds to scale ratio *R* of 2275, indicating that in the lower troposphere the ISR can extend over three decades in the TKE spectrum.

Figures 6a and 6b respectively show 1/Pr_t and Pr_t plotted against Ri. The two panels present the same information but in two different formats. Figure 7a uses the log-linear scale format for easier comparison with Hocking and Mu (1997), which is popular among radar scientists, whereas Fig. 7b uses the log-log format that is compatible with Canuto et al. (2008) and Kantha and Carniel (2009), which is familiar to atmospheric scientists and oceanographers. The cyan circles denote ShUREX 2016 observations. Blue circles are from laboratory experiments (Strang and Fernando 2001; Ohya 2001; Rehmann and Koseff 2004), direct-numerical-simulation numerical-model results of Stretch et al. (2001), and large-eddy-simulation model results of Zilitinkevich et al. (2007, 2008), as presented in Canuto et al. (2008) and Kantha and Carniel (2009). Red circles are from observations in the atmosphere (Kondo et al. 1978; Gossard and Frisch 1987; Bertin et al. 1997).

It can be seen that ShUREX observations (cyan circles) are in good agreement with the earlier studies. The large scatter seen is typical of measurements such as these (see large circles from earlier studies, exhibiting a similar degree of scatter). The thin red line corresponds to

$$Pr_t^{-1} = (3.6Ri)^{-1}, (53)$$

as in Gossard and Frisch (1987). The thin black line corresponds to

$$\Pr_t^{-1} = [(1 + B_\theta \gamma) Ri]^{-1},$$
 (54)

with a constant value for γ of 1.95. From Eq. (36), it can be seen that

$$\Pr_t^{-1} \to \frac{R_f^{\max}}{\text{Ri}} \quad \text{as} \quad \text{Ri} \to \infty$$
 (55)

so that Eqs. (53) and (54) are equivalent to assuming Ri is large and $R_f^{\text{max}} = 0.28$ and 0.14, respectively. Although the scatter in observational data is large, Eq. (54) is



FIG. 5. Turbulence activity (also known as "buoyancy Reynolds number") plotted against gradient Richardson number Ri. From left to right, the vertical lines are for Ri = 0.09, 0.25, 0.5, and 1.0.



FIG. 6. (a) Inverse of the Prandtl number plotted against gradient Richardson number. See the text for details. The plot uses the log–linear scale format of Hocking and Mu (1997) for easier comparison. Cyan circles denote ShUREX 2016 measurements. Large blue circles show data from earlier studies in the laboratory and numerical simulations. Large red circles show measurements in the atmosphere. For more details, see the text. The thick blue and black lines correspond to the semiempirical law of Eq. (36), whereas the thick red line corresponds to the second-moment closure model of Kantha and Carniel (2009). Thin red and black lines correspond to Eqs. (53) and (54). The thin black line at the top corresponds to Businger et al. (1971). (b) As in (a), but for the Prandtl number plotted against gradient Richardson number using the log–log scale format of Canuto et al. (2008) and Kantha and Carniel (2009) for easier comparison.

consistent with observational data as long as Ri values are higher than approximately 0.25. However, both Eqs. (53) and (54) do not behave well at Ri values below about 0.25, yielding Prandtl numbers well below a value of unity. It is well known from numerous laboratory experiments that in neutrally stratified turbulent flows (Ri = 0) the Prandtl



FIG. 7. As in Fig. 6, but the (a) flux Richardson number and (b) mixing coefficient are plotted against the gradient Richardson number (see text for details).

number is around 0.8. Equations (53) and (54) do not have the proper asymptotic behavior as $Ri \rightarrow 0$, whereas Eq. (35) (thick blue line) does:

$$\operatorname{Pr}_{t} \to \operatorname{Pr}_{t}^{0} < 1 \quad \text{as} \quad \operatorname{Ri} \to 0.$$
 (56)

The thick blue line in Figs. 6a and 6b corresponds to the semiempirical model of Eq. (36) with $R_f^{\text{max}} = 0.25$ and $Pr_t^0 = 0.8$, whereas the thick black line corresponds to $R_f^{\text{max}} = 0.17$ and $Pr_t^0 = 0.8$. These are close to the thick red line corresponding to theoretical results from the second-moment closure

model of Kantha and Carniel (2009), thus confirming the good agreement between the two. The closure model of Kantha and Carniel (2009) is consistent with laboratory and field observations as well as with recent theoretical studies (Galperin et al. 2007) that indicate that turbulence can exist at Ri values as high as 200.

Last, recall that the primary interest in studies involving measurements of the TKE dissipation rate, both in the ocean and the atmosphere, is in determining the scalar turbulent mixing coefficient in the fluid column through Eq. (20). This, of course, requires knowledge of mixing coefficient χ_m (equivalently R_f). For future reference, Figs. 7a and 7b show R_f and χ_m plotted against Ri. The observational data points are as in Figs. 6a and 6b. Once again, ShUREX observations are consistent with earlier studies.

It is worth pointing out that, while R_f and R_i are independent measurements, from Eq. (31) Pr_t involves Ri and therefore there could be some self-correlation in the Pr_t and $1/Pr_t$ plots against Ri. Anderson (2009) made a study of this topic, but the relationship he recommends [his Eq. (16)] for the variation of Pr_t versus Ri, based on his analysis (not shown), gives values in poor agreement with data in Figs. 6a and 6b. He also assumes Pr_t at Ri = 0 is equal to 1.0. Using a more realistic value of around 0.8, the agreement becomes worse. Nevertheless, the possibility of self-correlation should be kept in mind when interpreting inferred (and not directly measured) values of Pr_t in the oceans and the atmosphere. The possible effect of the differences in the molecular Prandtl number of air and water (Salehipour et al. 2015) should also be kept in mind.

Overall, the agreement between ShUREX data and earlier studies is very good, but scatter is still too large. The lack of collocation in time and space of UAV and radiosonde observations may have contributed to some but not all of the scatter observed in Figs. 6 and 7. Note also that some points fall beyond $Pr_t = 1$ and $Pr_t = 0$, both theoretically untenable. The same is true for some of the earlier studies. This goes to highlight the large uncertainty and hence error bars associated with difficult turbulence measurements such as these, whether in the oceans, the atmosphere, or the laboratory.

An important point to note in Figs. 6 and 7 is that the thick black line corresponding to the semiempirical model of Eqs. (36) and (35), respectively, but with $R_f^{\text{max}} = 0.17$ and $\Pr_t^0 = 0.8$, appears to agree better with data from both ShUREX and earlier studies for Ri values above approximately 0.1. This is interesting, since an R_f value of 0.17 corresponds to a χ_m value of 0.2. The various universal constants that go into Kantha and Clayson's (2004) and Kantha and Carniel's (2009) models determine the values of both R_f^{max} and \Pr_t^0 , and so this study indicates the need for perhaps reexamining one of those universal constants to reduce the value of R_f^{max} from the currently set value of 0.25 to 0.17.

Last, it is important to remember that ultimately, a primary goal of turbulence models and measurements is to be able to better determine and utilize the mixing coefficients of momentum and heat (and scalar properties), K_M and K_{θ} , respectively, in the oceans and the atmosphere. These coefficients can be written in nondimensional form, using Eqs. (13), (20), (29), and (31), as

$$\overline{K}_{M} = \frac{K_{M}N^{2}}{\varepsilon} = \frac{\mathrm{Ri}}{1 - R_{f}} \quad \text{and} \quad \overline{K}_{H} = \frac{K_{\theta}N^{2}}{\varepsilon} = \frac{R_{f}}{1 - R_{f}}.$$
(57)

Because R_f is a unique function of Ri (e.g., Kantha and Carniel 2009), both of these nondimensional coefficients are functions of Ri and only Ri. In the oceans, the mixing coefficient K_M can be deduced from microstructure measurements, provided that Ri is also measured simultaneously (mixing coefficient K_H is obtained from simultaneous measurements of the dissipation rate of the temperature variance χ_T by the microstructure profiler). This once again highlights the importance of deploying ADCPs during microstructure measurements if Ri values cannot be obtained from the sensors deployed on the profiler. For UAV measurements in the atmosphere, on the other hand, it is important to be able to deduce ambient wind velocity as accurately as possible (currently still problematic) from measurements of velocities relative to the wind and the ground.

4. Concluding remarks

From measurements made over the past few decades, oceanographers have discovered that tracer experiments in the upper ocean show that an excellent agreement is obtained for tracer diffusion if the mixing coefficient χ_m is assumed to be 0.20. However, theory requires that it be a function of the strength of stratification as indicated, for example, by the gradient Richardson number Ri. The constant mixing coefficient producing good agreement with tracer studies in the ocean has puzzled oceanographers for decades [see the reviews by Peltier and Caulfield (2003); Gregg et al. (2018)]. ShUREX 2016 observations reported above are consistent with past studies in the oceans, the atmosphere, and the laboratory. The histogram of χ_m shows that the most likely value is about 0.16, and use of the corresponding value of γ in radar studies is a viable option, just like the use of $\chi_m = 0.2$ provides acceptable diffusivities in the ocean.

It is well known that χ_m can have a value as high as 0.8 during the initial stages of Kelvin–Helmholtz instability before fully developed turbulence ensues and χ_m settles down to a value of about 0.2 (e.g., Peltier and Caulfield 2003). It is also well known that accurate measurements of diffusion and dissipation rates in stably stratified flows are difficult to make and that data points necessarily involve huge error bars, which are often not presented. Therefore, given the large scatter, the Ri dependence of χ_m is often obscured by the scatter (e.g., Fig. 7b), and a constant value can be taken as a reasonable fit to the data as long as Ri values exceed about 0.1 or so. It may be that

Ri seldom falls below approximately 0.1 in the oceans and the atmosphere so that a value for χ_m of about 0.2 turns out to be a good approximation, all things considered. However, this is just speculation, and further studies and observations are essential to reinforce or refute it. We suggest that any future observations, whether in the oceans, the atmosphere, or the laboratory, include simultaneous measurements of Ri. This recommendation means that any future tracer studies in the ocean should also simultaneously measure prevailing Ri values. If it turns out that Ri seldom falls below approximately 0.1 but can reach values well above the canonical value of 0.25, then the above speculation may be justifiable.

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