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Surrogate Modeling of Aerodynamic Simulations for Multiple Operating Conditions Using Machine Learning

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This paper describes a methodology, called local decomposition method, which aims at building a surrogate model based on steady turbulent aerodynamic fields at multiple operating conditions. The various shapes taken by the aerodynamic fields due to the multiple operation conditions pose real challenges as well as the computational cost of the high-fidelity simulations. The developed strategy mitigates these issues by combining traditional surrogate models and machine learning. The central idea is to separate the solutions with a subsonic behavior from the transonic and high-gradient solutions. First, a shock sensor extracts a feature corresponding to the presence of discontinuities, easing the clustering of the simulations by an unsupervised learning algorithm. Second, a supervised learning algorithm divides the parameter space into subdomains, associated to different flow regimes. Local reduced-order models are built on each subdomain using proper orthogonal decomposition coupled with a multivariate interpolation tool. Finally, an improved resampling technique taking advantage of the subdomain decomposition minimizes the redundancy of sampling. The methodology is assessed on the turbulent two-dimensional flow around the RAE2822 transonic airfoil. It exhibits a significant improvement in terms of prediction accuracy for the developed strategy compared with the classical method of surrogate modeling.

Nomenclature

A	=	matrix of the reduced coordinates	S	=	matrix of the snapshots
a_k	=	k th reduced coordinate	s_i	=	quantity of interest at node i
B	=	matrix of the reduced coordinates of the sensor	T	=	temperature
b_k	=	k th reduced coordinate of the sensor	U	=	velocity
C	=	chord length	w	=	weight of the Gaussian mixture model
C_k	=	k th cluster	X	=	horizontal coordinate along the chord
C_f	=	friction coefficient	Y	=	vertical coordinate
C_p	=	pressure coefficient	y	=	target value
d	=	dimension of the quantity of interest	α	=	angle of attack
E	=	averaged normalized error	γ	=	expectation of posterior probability
f	=	high-fidelity model	Γ	=	spatial domain
g	=	acceleration due to the gravity or normal distribution	δ	=	Kronecker symbol
H	=	global entropy	ϵ	=	energy ratio
h	=	altitude	θ	=	hyperparameters
L	=	temperature lapse rate	λ	=	eigenvalues matrix
I	=	latent function matrix	λ	=	eigenvalues
l	=	latent function	μ	=	mean of the Gaussian process
M	=	Mach number	ρ	=	density
m	=	number of predictions	Σ	=	covariance matrix
\mathcal{N}	=	Gaussian probability distribution	σ_0^2	=	prior covariance
n	=	number of training samples	σ	=	sigmoid function
p	=	dimension of an input parameter or static pressure	τ_w	=	wall shear stress
Q_2	=	predictivity coefficient	Φ	=	mixture coefficient
q	=	number of clusters	ϕ	=	proper orthogonal decomposition matrix
r	=	specific gas constant or correlation function	χ	=	input parameter
			$\mathbb{1}_C$	=	hard splitting function

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Subscripts

p	=	prediction
t	=	training
0	=	sea level
∞	=	freestream

Superscripts

(k)	=	k th component or element
$'$	=	fluctuating part

$\tilde{\cdot}$	=	surrogate model
$\bar{\cdot}$	=	mean
$ \cdot $	=	absolute value
$\ \cdot\ _2$	=	Euclidian norm
(\cdot, \cdot)	=	canonical inner product

I. Introduction

OVERALL aircraft design and optimization rely increasingly on numerical simulations for structural, aerodynamics, or even noise analysis. Particularly, the computational fluid dynamics (CFD) plays a significant role in solving Navier–Stokes equations, in order to predict vector-valued functions of specific quantities of interest, such as wall pressure field. The equations are discretized into algebraic systems that lead to prohibitive computational cost for simulations with a high number of degrees of freedom. Moreover, the inflow conditions may vary and form a multidimensional parameter space. Its full exploration requires the computation of a very large number of expensive simulations and becomes intractable. One of the main solutions to overcome this problem is the substitution of the high-fidelity simulations by a mathematical approximation much faster to be run, referred to as a surrogate model. It represents an interesting trade-off between precision and computation time. Furthermore, reducing the computational time of the exploration for high-fidelity CFD can open the way to multiphysics simulations using surrogate models for the fluid parts.

The surrogate modeling of high-dimensional vector-valued functions is mainly performed with a reduced-order approach, called reduced-order modeling (ROM). Originally developed for the study of coherent structures in the turbulent boundary layer [1], ROM methods have shown various applications, such as aeroelasticity [2], optimal flow control [3], turbulent flows [4,5], or geophysics [6]. Most ROM methods are applied to CFD problems by approximating the high-fidelity model as a linear combination of low-dimensional basis vectors, weighted by purposely tuned parameters. The basis vectors characterize the main features of the system behavior. Proper orthogonal decomposition (POD) is a particular and very popular method of dimension reduction used very frequently for CFD problems. It computes the basis vectors and the corresponding modal coefficients with an optimal least-square approach from a given number of high-fidelity computations, also called snapshots, at different state parameters. The ROM coefficients are calculated only for a finite and discrete number of input parameters, whereas the surrogate model is evaluated on a new parameter set. Thus a continuous representation of the coefficients over the whole state-parameter space has to be provided in order to build the final model, leading to two different approaches:

1) The intrusive ROM resolves the governing equations by projecting them into a set of basis function of smaller dimension, leading to a system of ordinary differential equations for the coefficients. The projection-based methods have the advantage to retain some of the physics from the governing equations and to give rigorous error bounds and error estimation [7]. However, both stability and accuracy issues can occur [8]. By their intrusive nature, these methods modify also the source code of the high-fidelity model, leading to substantial modifications, if not impossible, when commercial software packages are used. Moreover, the reduced equations are solved on the whole domain and for all the conservative variables even if the quantities of interest are evaluated on a subdomain and for a small number of variables. The high-Reynolds-number turbulent flows [9,10] give an example of challenging and active field of research for projection-based ROM. More information on intrusive ROM can be found in Ref. [11].

2) The second method, the nonintrusive data fitting ROM, does not need any knowledge about the high-fidelity model, considered as a black box, allowing to deal with very complex physics. Instead of manipulating the governing equations, the value of the coefficients are predicted by methods of multidimensional data fitting such as polynomial regression, radial basis function, or Gaussian process regression [12]. Nonintrusive ROM has been successfully applied

in CFD, for instance, in aero-icing problems [13], uncertainties quantification for urban flow [14], or steady aerodynamics [15–17]. One can note that hybrid methods mixing projection-based and nonintrusive approaches have been developed by solving an inverse problem, where the coefficients of the reduced-order governing equations are inferred using the output of the simulations [18].

Here, only nonintrusive data fitting are considered and the high-fidelity model is treated as a black box.

Despite the usefulness of the energy-ranked POD and its extensive use, some limitations have been observed [19]. Indeed, low-energy perturbations can be masked although they could be representative of a part of the system behavior. Problems with bifurcations can have typical characteristics, such as aerodynamic flows with varying inflow conditions leading to either subsonic or transonic regime. In these cases, the classical method computing the dominant modes in a single POD basis fails to produce accurate responses for predictions in highly nonlinear region and not directly in the neighborhood of the snapshots [20,21]. The mix of the different physical regimes in the POD basis vectors can explain this problem. Indeed, small errors in the multivariate interpolation step can amplify POD modes associated with a physical regime that does not exist for the considered prediction. For this reason, approaches based on local reduced-order models have emerged in the literature by considering only restrictions to the total amount of snapshots [22–28]. This paper describes an original active local method, called “local decomposition method” (LDM), extending the classical reduced-order modeling method using POD and data fit method to particular steady problems with different physical regimes.

The method proposed here computes local subspaces of the state-parameter space by combining a physical-based sensor with machine learning tools. The physical-based sensor is a central element of the method to achieve proper separations of the physical regimes. Indeed, the conversion of the vector-valued output into a vector of physical-based features gives the possibility to cluster the snapshots into subsets with the same physical behavior. Thus the POD basis vectors are more representative of the physics. A shock sensor is used for the particular problems mixing subsonic and transonic conditions. It measures the nonlinearities and sharp gradients of the flow field. As the different phenomena are no more mixed in the POD basis, building a local reduced-order model on each of these subsets achieves a better consideration of the physical regimes. The clustering of the snapshots provides also a greater flexibility to the data fit model that can behave independently on each subgroup. As regard the prediction of untried sets of parameters, a supervised learning algorithm associates each region of the parameter space with a local reduced-order model and its respective subspace, allowing to map the input parameter space to the right physical regime. This last step is called input space decomposition.

Replacing the global POD basis with several local POD bases is a relatively recent development for parametric reduced-order modeling [23,24,27,28] and may seem counterintuitive. Indeed, the compressive capability of the POD may be weakened by increasing the number of bases, and the robustness of each data fit method can decrease with the reduction of training samples due to the repartition of these latter on the different models. On the contrary, the local models enable a clear separation of the phenomena improving the prediction of the surrogate model. Moreover, as underlined in [29], the POD shows elliptic properties while aerodynamics is characterized by hyperbolic equations. Therefore, a local approach can demonstrate similarities with discontinuous Galerkin method to tackle hyperbolic problems. In this work, only Gaussian process regression (GPR) is investigated as a method of data fitting. Thus the terms “POD/data fitting” and “POD/GPR” are used indifferently to refer to the classical nonintrusive ROM.

This paper aims to present a local reduced-order model built with machine learning tools and using a physical-based approach in order to address parameter-dependent problems with either subsonic or transonic regime. It is organized as follows: Sec. II gives an overview of the classical nonintrusive POD/data fitting approach. Then, Sec. III introduces the LDM with its underlying principles based on machine learning. Then, results from a one-dimensional analytical case and two-dimensional transonic airfoil are presented in Sec. IV, demonstrating the capability of the LDM to deal with different physical regimes, including shock waves. Finally, Sec. V provides a summary and the conclusions.

II. Nonintrusive POD/Data Fitting Reduced Order Modeling

First, some notations are introduced. One considers a real vector-valued function f representing the high-fidelity model defined from \mathbb{R}^p to \mathbb{R}^d , where p is the number of parameters and d the dimension of the vector-valued quantity of interest. For example, a CFD code predicting the wall pressure field of an airfoil for different values of Mach number and angle of attack defines an input domain with p equal to 2 and d corresponding to the number of nodes representing the wall. Similarly, f represents the vector-valued surrogate model with the same domain of definition from \mathbb{R}^p to \mathbb{R}^d . The matrix of the training input parameters is noted $\mathcal{X}_t = [\mathcal{X}_{t_1} \dots \mathcal{X}_{t_n}]^T \in \mathbb{R}^{n \times p}$, where n is the number of training samples, and \mathcal{X}_{t_i} is the i th vector of the parameter set, which can be written with its components as $\mathcal{X}_{t_i} = [\mathcal{X}_{t_i}^{(1)} \dots \mathcal{X}_{t_i}^{(p)}]$. In the same way, the matrix of the test samples, also referred to as untried input parameters or merely the predictions, is noted: $\mathcal{X}_p = [\mathcal{X}_{p_1} \dots \mathcal{X}_{p_m}]^T \in \mathbb{R}^{m \times p}$, with m the number of predictions. S_i designates the vector of the i th snapshot such that $S_i = f(\mathcal{X}_{t_i}) \in \mathbb{R}^d$ and S_i defines the matrix of the training snapshots $S_t = [S_1 \dots S_n]^T \in \mathbb{R}^{n \times d}$. The terms \bar{S}_t and \bar{f} are used interchangeably to refer to the mean snapshot $\bar{S} = \bar{f} = (1/n) \sum_{k=1}^n S_k \in \mathbb{R}^d$. The fluctuating part S'_i of the training snapshots is defined by the snapshots matrix where the mean snapshot has been removed such that $S'_i = [S_1 - \bar{S} \dots S_n - \bar{S}]^T$. The first mode of data with nonvanishing mean is very close to the mean value of the snapshots for reasonable variations in the data. For this reason, the POD is performed on the fluctuating quantity S'_i .

The nonintrusive POD/data-fit reduced order modeling is made of three steps: the generation of the initial training samples, the POD dimension reduction, and the interpolation of the POD coefficients. All of them are described in the following parts. The whole process of the method is depicted in Fig. 1. One can note that the POD/GPR method is the common basis of the further developments presented in this paper and serves as a reference for the method assessment performed in Sec. IV.

A. Sampling Plans

The purpose of the surrogate model is to simulate the input/output behavior over the domain of variation of the parameters based on a limited number of high-fidelity evaluations. Correct predictions are required not only for the design points but also at all off-design conditions. For this reason, the limited number of snapshots should be optimally placed in order to build a model capturing the maximum amount of information about the physics over the parameter space.

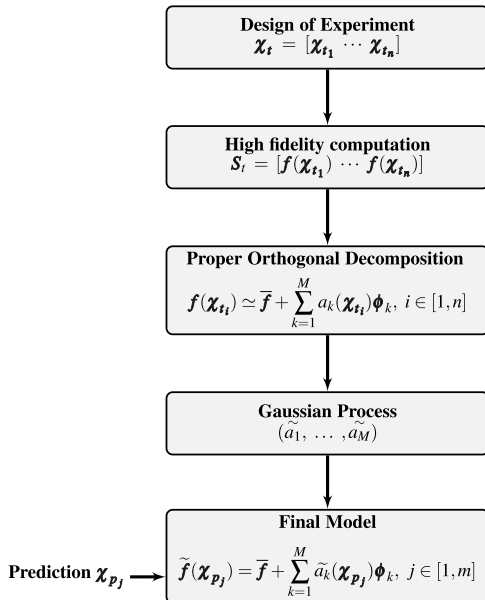


Fig. 1 Flowchart of the POD/GPR method.

An inappropriate repartition of the input parameters could lead to a surrogate model with large discrepancies. To the extent possible, the number of snapshots will be limited to the rule of thumb $10p$ studied by Loeppky et al. [30], where p is the number of parameters.

Contrary to the projection-based method, the nonintrusive POD/GPR approach does not have access to prior information on the system given by the coefficients of the governing equations [31]. The critical issue of the choice of the a priori training snapshots is called design of experiment (DOE). As explained previously, the main goal of the DOE is to generate well-distributed samples in the parameter space to give sufficient information to the learning process. DOE methods have been widely studied in the literature providing many techniques for experimental parametric studies and computer experiments. One can cite for example random and orthogonal array methods with Monte Carlo and Latin Hypercube Sampling [32], geometrical approaches such as centroidal Voronoi tessellations [33], or low-discrepancy sampling techniques such as Halton, Sobol, or Faure sequences [34]. In the present work, low-discrepancy sequences have been adopted due to their iterative design. Indeed, the number of samples can be extended on purpose, and high-density regions can be easily defined while keeping the space-filling properties. Both properties are very interesting features for active learning. The other deterministic methods require a preset number of samples and cannot be extended without losing a part of their space-filling property.

B. Proper Orthogonal Decomposition

The POD is an efficient technique of dimension reduction based on spectral decomposition for high-dimensional, multivariate, and nonlinear data set. A wide range of applications can be found in the literature, such as human face characterization [35], data compression [36], and optimal control [37]. The POD term was first introduced in 1967 [38] to study dominant turbulent eddies, also called coherent structures. POD is also known as Karhunen-Loève decomposition, Hotelling analysis, or principal component analysis, in other fields of application. Among all the possible linear decompositions of the high-fidelity function, the POD method minimizes in a least square sense the residual of the projection of the high-fidelity model, yielding an optimal basis in terms of the representativeness of the data [39]. The least square problem is equivalent to a maximization problem [4,39]. Introducing the canonical inner product (\cdot, \cdot) on \mathbb{R}^d , the POD basis is the solution of the following formulation:

$$\begin{aligned} \max_{\phi_1, \dots, \phi_n} \sum_{i=1}^n \sum_{j=1}^n |(S'_i, \phi_j)|^2 \\ \text{subject to } (\phi_i, \phi_j) = \delta_{i,j} \end{aligned} \quad (1)$$

where $\phi_i \in \mathbb{R}^d$ is the i th vector basis, S'_i the fluctuating part of the i th snapshot, and $\delta_{i,j}$ the Kronecker symbol satisfying $\delta_{i,j} = 1$ for $i = j$ and $\delta_{i,j} = 0$ otherwise. The matrix of the vector basis $\phi \in \mathbb{R}^{n \times d}$ is introduced such that $\phi = [\phi_1 \dots \phi_n]^T$.

The method of snapshots proposed by Sirovich [40] is employed to solve the maximization problem in Eq. (1) and leads to an eigenvalues problem:

$$\frac{1}{n} S'_t S'^T_t = \phi \lambda \phi^T \quad (2)$$

where $\lambda \in \mathbb{R}^{d \times d}$ is the diagonal matrix of the eigenvalues associated to the matrix of the eigenvectors ϕ . The eigenvalues problem can be solved either by an eigen decomposition or a singular values decomposition (SVD). The latter gives a better precision for the smaller eigenvalues and provides an iterative approach well-fitted for resampling. One can note that the self-adjoint operator property of $S'_t S'^T_t$ ensures that the computed POD modes form a complete orthonormal set built as $\{\phi_1, \dots, \phi_n\}$, on which the high-fidelity model is decomposed:

$$f(\mathcal{X}_{t_i}) = \bar{f} + \sum_{k=1}^n a_k(\mathcal{X}_{t_i}) \phi_k, \quad \forall i \in [1, n] \quad (3)$$

where $a_k(\chi_{t_i}) \in \mathbb{R}$ is the reduced coordinate associated with the k th POD mode $\phi_k \in \mathbb{R}^d$. All the reduced coordinates are computed using the orthonormality property of the POD basis and are expressed as:

$$a_k(\chi_{t_i}) = (S'_i, \phi_k) \quad (4)$$

The POD is optimal in terms of energy and provides an energy-ranked basis. Usually, the dimensional space of the snapshots is sparse in an L_2 sense. Therefore, only a small number of the most energetic POD modes can be retained in order to reduce the dimension of the system. The smallest eigenvalues are neglected, leading to a truncation of the basis. This heuristic criterion can be written more formally as a minimum ratio of the captured energy, which means finding the number M of kept basis vectors such that for a given amount of energy ratio ϵ :

$$\frac{\sum_{k=1}^M \lambda_k}{\sum_{j=1}^n \lambda_j} > \epsilon \quad (5)$$

A classic ratio of energy present in the literature is 0.99 [3,40]. Once M has been set, the truncated linear combination of the eigenfunctions gives the approximation of the high-fidelity model:

$$f(\chi_{t_i}) \simeq \bar{f} + \sum_{k=1}^M a_k(\chi_{t_i}) \phi_k \quad \forall i \in [1, n] \quad (6)$$

C. Interpolation with Gaussian Process Regression

The interpolation is the next step of the POD/GPR surrogate model. The reduced coordinates a_k have been computed at a small number of training parameters, whereas the analysis of the high-fidelity model for various inflow conditions requires a continuous evaluation over the input parameter space. Thus, the values of the reduced coordinates at untried parameter combinations are estimated with a data-fit method. The most popular methods in the surrogate modeling literature are formed of polynomial regression, radial basis function, or Gaussian process regression (GPR) [12]. A particular emphasis is given to this latter method. It has been employed in this paper due to its capability to deal with nonlinear problems, its high flexibility, and the provided error estimation of the predictor. GPR is also called “kriging” and has been first applied in geostatistics [41]. The short overview of the GPR in this paper is introduced following the formalism of Rasmussen [42] and is directly applied to the continuous representation of the reduced coordinates. They are assumed to follow a Gaussian process, which is outlined by a collection of random variables having a joint Gaussian distribution of mean μ and covariance matrix Σ . If the reduced coordinate a_k follows a Gaussian process, it reads:

$$A_t^{(k)} \sim \mathcal{N}(\mu^{(k)}, \Sigma^{(k)}) \quad (7)$$

with $A_t^{(k)} = [a_k(\chi_{t_1}) \dots a_k(\chi_{t_n})]^T$ defining the matrix of the k th reduced coordinate at training parameters, and $A_p^{(k)} = [a_k(\chi_{p_1}) \dots a_k(\chi_{p_m})]^T$ the predictions at the unknown combinations of parameters. In the interests of simplifying notation and analysis, the index k is removed and becomes implicit. The joint distribution of the reduced coordinates at training and unknown parameters is given by:

$$\begin{bmatrix} A_t \\ A_p \end{bmatrix} \sim \mathcal{N}\left(\begin{bmatrix} \mu_t \\ \mu_p \end{bmatrix}, \begin{bmatrix} \Sigma_{tt} & \Sigma_{tp} \\ \Sigma_{pt} & \Sigma_{pp} \end{bmatrix}\right) \quad (8)$$

with Σ_{tp} the covariance matrix between χ_t and χ_p . The central issue of the GPR remains to be addressed, namely, how to determine the means and the covariance between the inputs. A classical stationarity assumption is that the correlation depends only on the magnitude of the Euclidean distance between the two input parameters but not on the values themselves, such that the i, j th element of the covariance matrix is given by:

$$[\Sigma_{tp}]_{i,j} = \sigma_0^2 r(\|\chi_{t_i} - \chi_{p_j}\|_2) \quad \forall i, j \in [1, n] \times [1, m] \quad (9)$$

with σ_0^2 the prior covariance corresponding to the level of uncertainty for predictions far from the training data and r the correlation function. The latter is usually monotonically decreasing with $r(0) = 1$. A wide range of functions have been proposed to model the relation between the covariance and the input distance, such as radial basis function, Matern, or periodic regression function [42]. The anisotropic radial basis function, chosen for our problem, is one the most classical model of the regression functions due to its smoothness, infinite differentiability, and analytical derivability. Its expression introduces the hyperparameter $\theta_k \in \mathbb{R}^+$ and is given by:

$$r(\|\chi_{t_i} - \chi_{p_j}\|_2) = \prod_{k=1}^p \exp\left(\frac{-\|\chi_{t_i}^{(k)} - \chi_{p_j}^{(k)}\|_2}{2\theta_k}\right) \quad \forall i, j \in [1, n] \times [1, m] \quad (10)$$

The hyperparameter θ_k defines the way the data are explained by the component k of the input parameters. Small values mean that the correlation is high between the inputs and the model is very sensitive to the dimension k . On the other hand, large values of θ_k illustrate a model slowly varying with the data.

The final form of the predictor is derived using the conditional distribution of A_p , given A_t , also called a posteriori distribution that is still Gaussian and written as:

$$p(A_p | A_t) \sim \mathcal{N}(\mu_p + \Sigma_{pt} \Sigma_{tt}^{-1} (A_t - \mu_t), \Sigma_{pp} - \Sigma_{pt} \Sigma_{tt}^{-1} \Sigma_{tp}) \quad (11)$$

The mean of the distribution gives the final value of the predictions at the untried set of parameters. Regarding the variance, it provides an estimate of the possible range taken by the prediction, which can also be seen as the mean-square error. The latter has the interesting feature not to be dependent on the value of the output but only to the input parameters. Both θ_k and σ_0^2 remain to be determined in order to obtain the final prediction. They are computed during the training phase of the GPR, most of the time by a maximum likelihood estimation (MLE) approach or a leave-one-out method [42]. Martin and Simpson [43] have shown that the MLE works better than leave-one-out in general. For this reason, MLE is applied in the GPR/POD method, solving numerically the nonlinear maximization problem of the log-likelihood:

$$\log(p(A_t | \theta)) = -\frac{1}{2} A_t^T \Sigma_{tt}^{-1} A_t - \frac{1}{2} \log |\Sigma_{tt}| - \frac{n}{2} \log(2\pi) \quad (12)$$

where $|\cdot|$ denotes the determinant operator. The partial derivatives of the marginal likelihood with regard to the hyperparameters can be analytically derived. Thus, it is possible to use a gradient-based optimization algorithm in order to numerically find a local solution to the MLE problem. The Limited-memory Broyden-Fletcher-Goldfarb-Shanno Bounded (L-BFGS-B) algorithm [44] is employed in this paper to determine the hyperparameters. This popular quasi-Newton method handles simple bound constraints and is coupled with random restarts to avoid local maximum of bad quality.

By assuming that the POD basis vectors are invariant with respect to the input parameters, the final surrogate model predicts the quantity of interest at the j th untried input parameter χ_{p_j} such that:

$$\tilde{f}(\chi_{p_j}) = \bar{f} + \sum_{k=1}^M \tilde{a}_k(\chi_{p_j}) \phi_k, \quad \forall j \in [1, m] \quad (13)$$

with $\tilde{a}_k(\chi_{p_j}) = [\mu_p^{(k)} + \Sigma_{p,t}^{(k)} \Sigma_{tt}^{(k)-1} (A_t^{(k)} - \mu_t^{(k)})]_j$ the approximation of the weighting coefficient a_k over the parameter space. The a priori mean $\mu_p^{(k)}$ is usually considered equal to zero as the training data have been standardized with zero mean. One can note that different versions of GPR or kriging can be used, such as Bayesian kriging [45]. Here, the Python library scikit-learn [46] is employed to generate the GPR models.

III. Local Decomposition Method

As explained in Sec. I, the LDM proposed in this paper extends the classical POD/GPR reduced-order modeling by employing a local approach, inspired by the mixture of experts [27] and dynamic local reduced-order modeling [23]. Instead of a unique global POD basis, several local bases are computed using machine learning tools yielding to more flexible behaviors bringing out a precise delimitation of the physical regimes. First, a shock sensor computes specific features for all the snapshots. Then, the latter are clustered into different subsets thanks to the shock features. Finally, the parameter space is divided into several domains according the clustering of the snapshots. The Fig. 2 sketches the process. One can note that a comparable approach has been used for aero-icing certification [28]. The specificity of the presented method includes, besides the introduction of a feature extraction with a shock sensor, a novel resampling strategy and the application to an aerodynamics case. The active resampling is carried out by identifying the subspaces with the highest entropy. Extra snapshots are added in these specific subspaces with the objective to minimize the redundancy of the sampling, thus increasing the accuracy of the surrogate model. The Fig. 3 illustrates the whole method.

A. Coupling Machine Learning Tools with a Physical Sensor

Let us introduce basic machine learning vocabulary. Learning problems can be divided into two distinctive categories: *supervised* and *unsupervised*. Here, the machine learning library *scikit-learn* [46] is employed in the in-house JPOD code to perform both supervised and unsupervised learning. In the context of supervised learning, some input variables have an influence on one or more outputs. This set of inputs and outputs forms a learning base, and the supervised learning simulates the input/output behavior using the learning base. The final goal is to predict the values of the outputs for untried inputs. The nature of the output subdivides the supervised learning into two subcategories: the classification, dealing with categorical input variables, and the regression, which is applied on real and continuous input variables. The GPR is an example of regression. As regard the unsupervised learning, the training set consists only of the input vectors without any corresponding outputs. Thus the purpose of the unsupervised learning is to identify underlying structures hidden in the parameter space but the accuracy of the algorithm cannot be defined by any objective function.

1. Physical-Based Shock Sensor to Detect Flow Regimes

The choice of the quantity characterizing the physical regimes, on which the clustering is performed, is a question of central importance impacting the quality of the classification. Usually, the unsupervised learning clusters directly the quantity of interest into groups with patterns of small differences [23,24,28]. However, the aim of the clustering in this paper is the physical regime separation, and the previous approach can lead to classification error. Indeed, two fields of the quantity of interest can have large differences even though they belong to the same physical regime. A classical method fails to separate them accurately. For this reason, this section proposes another method to perform the clustering. Based on a physical approach, a mathematical transformation converts the quantity of interest into a sensor of the physical regime. The main goal is to sharply quantify the physical regime to ease the clustering of the snapshots.

The application of this paper involves external aerodynamics with subsonic and transonic regimes, characterized by shock waves.

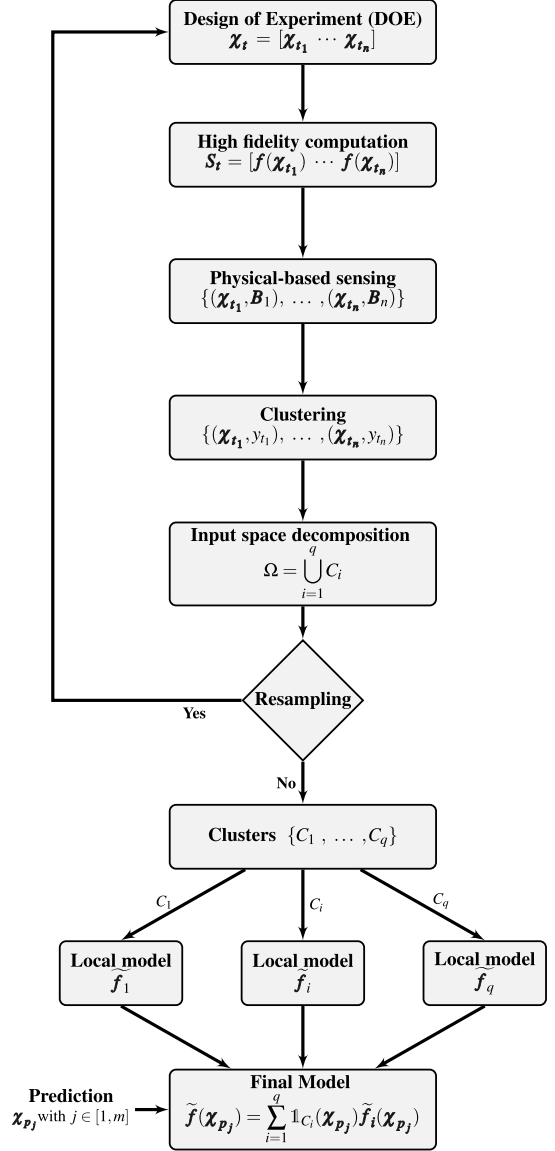


Fig. 3 Flowchart of the LDM.

A straightforward idea is to consider a shock sensor that is able to detect large changes in the variation of the quantity of interest, such as Jameson's shock sensor [47]. The latter has been developed as a heuristic method for nonoscillatory shock capturing numerical schemes. It is related to the second-order derivative of the pressure. However, the quantity of interest is not limited to pressure signals and a more general expression is introduced as:

$$\nu_i = \frac{|s_{i-1} - 2s_i + s_{i+1}|}{\epsilon_0 + |s_{i-1}| + 2|s_i| + |s_{i+1}|}, \quad \forall i \in [2, d-1] \quad (14)$$

where ν_i is the generalized sensor, ϵ_0 is a constant avoiding division by 0, and s_{i-1} , s_i , and s_{i+1} are the quantity of interest at, respectively, node $i-1$, i , and $i+1$. The dimension of the generalized sensor can be

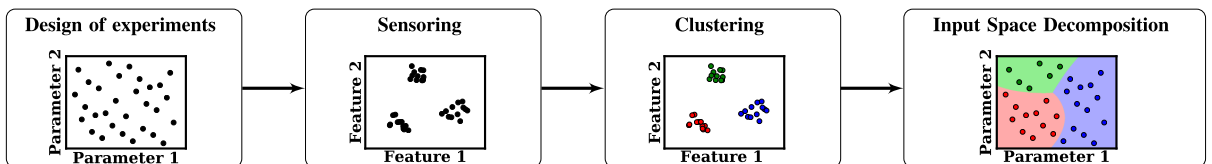


Fig. 2 Sketch of the LDM.

reduced by POD, such as the k th POD basis vector is associated to the reduced coordinates b_k . The latter can be interpreted as the representative quantity of the physical regime for a given snapshot. They are grouped in the vector \mathbf{B}_i defining the matrix $\mathbf{B} = [\mathbf{B}_1 \dots \mathbf{B}_n]^T$

2. Clustering of the Shock Sensors by Gaussian Mixture Model

The problem of identifying the inherent groupings in the input data refers to unsupervised classification, specifically clustering. K-means and Gaussian mixture model (GMM) are two well-known examples of algorithms classically employed to achieve clustering. This section puts a particular emphasis on GMM algorithm [48], where the main features are described.

Let us assume that the set $\{\mathbf{B}_1, \dots, \mathbf{B}_n\}$, characterizing the physical regimes, comes from q clusters C_1, \dots, C_q . Each cluster C_k follows a probability distribution of parameter θ_k and proportion w_k , regrouped for all the clusters in a mixture parameter $\Phi = [w_1 \dots w_q \theta_1 \dots \theta_q]$. The GMM algorithm consists in modeling \mathbf{B} with a mixture distribution of multivariate normal distributions g . Each one is associated with the cluster C_k such that the probability density function of \mathbf{B}_i is given by:

$$p(\mathbf{B}_i|\Phi) = \sum_{k=1}^q w_k g(\mathbf{B}_i|\theta_k), \quad \forall i \in [1, n] \quad (15)$$

, where the mixture weights w_k represent the probability that the observation comes from the k th Gaussian distribution and θ_k gives the mean and the covariance of the multivariate normal distribution g .

These mixture parameters regrouped in Φ are estimated iteratively using an Expectation Maximization algorithm (EM algorithm) [49]. The expectation of the posterior probability γ_k of belonging to the cluster k can be expressed with Bayes' theorem (E-step):

$$\gamma_k(\mathbf{B}_i) = p(C_k|\mathbf{B}_i) = \frac{p(\mathbf{B}_i|C_k)p(C_k)}{P(\mathbf{B}_i)} = \frac{w_k g(\mathbf{B}_i|\theta_k)}{\sum_{l=1}^q w_l g(\mathbf{B}_i|\theta_l)}, \quad \forall k \in [1, q], \quad \forall i \in [1, n] \quad (16)$$

Then, the mixture parameters can be re-estimated (M-step):

$$\mu_k = \frac{\sum_{i=1}^N \gamma_k(\mathbf{B}_i) \cdot \mathbf{B}_i}{\sum_{i=1}^N \gamma_k(\mathbf{B}_i)}, \quad \forall k \in [1, q] \quad (17)$$

$$\Sigma_k = \frac{\sum_{i=1}^N \gamma_k(\mathbf{B}_i) \cdot (\mathbf{B}_i - \mu_k) \cdot (\mathbf{B}_i - \mu_k)^T}{\sum_{i=1}^N \gamma_k(\mathbf{B}_i)}, \quad \forall k \in [1, q] \quad (18)$$

$$w_k = \frac{1}{n} \sum_{i=1}^N \gamma_k(\mathbf{B}_i), \quad \forall k \in [1, q] \quad (19)$$

These two steps are iterated until convergence of the log likelihood. The cluster of each quantity \mathbf{B}_i can be determined using the previous probability expression. The training set is built by applying a hard splitting such that:

$$\{(\mathbf{x}_{t_1}, y_{t_1}), \dots, (\mathbf{x}_{t_n}, y_{t_n})\} \text{ with } y_{t_i} = \left\{ C_k \mid \max_{k \in [0, q]} p(C_k|\mathbf{B}_i) \right\}, \quad \forall i \in [1, n] \quad (20)$$

with y_{t_i} the target variable of the cluster. This training set is used to train a supervised learning algorithm, described in the following section, in order to link the input parameter of each quantity \mathbf{B}_i with a class of physical regime.

3. Input Space Decomposition Using Gaussian Process Classification

The decomposition of the input space into subspaces where a single physical regime drives the flow can be interpreted as a supervised classification problem. Indeed, the training set is provided

by the clustering phase and trains an algorithm assigning the k th untried input parameters \mathbf{x}_{p_j} ($j \in [1, m]$) to the categorical variable y_{p_j} , which can take the different values of the q classes C_1, \dots, C_q . The Gaussian process classification (GPC) is a classical method to deal with classification. The principal steps of the method for two-class problem are outlined in this section. The interested readers can refer to Rasmussen and Williams [42] and Bishop [50] for the straightforward generalization to K classes.

As the nature of the classification outputs is discrete, it clearly differs from the regression problems outlined previously with GPR. The main idea is to transform the output of a Gaussian process defined on the real axis into a probability lying in the interval $[0, 1]$ using a nonlinear activation function. A latent function l defined on the input parameter is introduced and we denote the latent vector by \mathbf{l} such that:

$$\mathbf{l} = [l_{t_1}, \dots, l_{t_n}] \text{ with } l_{t_i} = l(\mathbf{x}_{t_i}) \text{ and } l_{p_j} = l(\mathbf{x}_{p_j}), \quad \forall i, j \in [1, n] \times [1, m] \quad (21)$$

This function aims to provide a more convenient and tractable formulation of the model [42] and will be removed by integration. A Gaussian process prior with a zero mean and a covariance matrix Σ_l is placed on the joint distribution of the latent function l :

$$\begin{bmatrix} \mathbf{l} \\ l_{p_j} \end{bmatrix} \sim \mathcal{N}(\mathbf{0}, \Sigma_l) \quad (22)$$

As regard the two-class problem with C_0 and C_1 , the probabilistic prediction is directly computed by $p(y_{p_j} = C_0 | \mathbf{x}_{t_i}, y_{t_i}, \mathbf{x}_{p_j})$ because $p(y_{p_j} = C_1 | \mathbf{x}_{t_i}, y_{t_i}, \mathbf{x}_{p_j})$ is given by $1 - p(y_{p_j} = C_0 | \mathbf{x}_{t_i}, y_{t_i}, \mathbf{x}_{p_j})$. The conditioning on the input variables is intentionally let implicit. The probabilistic prediction is given by:

$$p(y_{p_j} = C_0 | y_{t_i}) = \int p(y_{p_j} = C_0 | l_{p_j}) p(l_{p_j} | y_{t_i}) dl_{p_j} \quad (23)$$

where $p(y_{p_j} = C_0 | l_{p_j}) = \sigma(l_{p_j})$, with σ the nonlinear activation function defined by the sigmoid function:

$$\sigma(x) = \frac{1}{1 + e^{-x}} \quad (24)$$

The integral expressed in Eq. (23) is analytically intractable due to the non-Gaussian likelihood of $p(l_{p_j} | y_{t_i})$ [42]. The expansion of the latter with the sum rule, product rule, and Baye's theorem gives:

$$p(l_{p_j} | y_{t_i}) = \int p(l | y_{t_i}) p(l_{p_j} | \mathbf{l}) d\mathbf{l} \quad (25)$$

where $p(l_{p_j} | \mathbf{l})$ is Gaussian. The non-Gaussian probability $p(\mathbf{l} | y_{t_i})$ requires specific approximations, such as variational inference, expectation propagation, or Laplace approximation [50]. Finally, the hyperparameters of the covariance matrix Σ_l need to be determined, for example, with the maximization of the log-likelihood, which also required to use the Laplace approximation due to non-Gaussian terms.

B. An Entropy-Based Active Resampling

Several methods have been coupled with surrogate models to generate an active reduced-order model: local methods and subspace methods form the two main different approaches. Local methods look for particular points that could improve the accuracy of the model. One can cite, for example, leave-one-out cross-validation [45] testing the sensibility of the surrogate model to each training sample. The more critical sample for the surrogate defines a neighborhood in which an extra snapshot is added. Another example of a local method, the maximum mean-squared error, uses the posterior estimation of variance from the GPR and adds the sample with the maximum value to the training set. Multifidelity can also be used to perform active

infill sampling [51]. Another type of method based on a subspace approach identifies particular low-dimensional structures in the input parameters where the quantity of interest shows a significant variability. One can cite, for example, active subspaces [52] or sensibility analysis [53].

The original strategy proposed in this paper is based on a subspace approach and aims at taking advantage of the input space separation into several subsets. Indeed, the input space decomposition has provided subgroups of smaller dimensions among which some subspaces of interest can be selected to perform the resampling. One proposes to use a criterion based on the compressibility of the information, coming from an analysis of the POD eigenvalues, in order to identify these relevant structures. As explained in the last section, the POD eigenvalue represents the relative information contained by the modes. The global entropy H measures the redundancy of this information and is introduced as [39]:

$$H = -\frac{1}{\log(n)} \sum_{k=1}^n p_k \log(p_k) \quad \text{with} \quad p_k = \frac{\lambda_k}{\sum_{i=1}^n \lambda_i} \quad (26)$$

If the entropy goes to zero, there is only one nonzero singular value. The data are compressed into a unique mode. On the other hand, the entropy is equal to one if all the information is distributed among the modes, meaning that no compression is possible. Between these two extreme values, the entropy increases with the number of fundamental modes. The active resampling of the LDM assumes that the entropy and the structures of the system with discontinuities or high gradients are directly correlated. Thus, the probability to find new modes with a nonnegligible amount of energy is expected to be greater for the cluster with the highest value of entropy than for any other cluster.

C. Recombination in a Global Model by Hard-Splitting

The final recombination step consists of assembling the local reduced-order models in a single composite global model. Starting from the q clusters, a simple weighted sum is calculated using a “hard” split:

$$\tilde{f}(\mathbf{x}_{p_j}) = \sum_{i=1}^q \mathbb{1}_{C_i}(\mathbf{x}_{p_j}) \tilde{f}_i(\mathbf{x}_{p_j}), \quad \forall j \in [1, m] \quad (27)$$

where

$$\mathbb{1}_{C_j}(\mathbf{x}) = \begin{cases} 1 & \text{if } j = \underset{i \in [1, q]}{\operatorname{argmax}} P(\mathbf{x} \in C_i) \\ 0 & \text{else} \end{cases} \quad (28)$$

and \tilde{f}_i refers to the classical POD/GPR model built on the i th cluster. This sum provides a continuous but not differentiable prediction of all the input space, leading to a global model. The differentiable predictions require to use differentiable weighting functions, which is not the case for $\mathbb{1}$. One can cite, for example, soft clustering [54], substituting $\mathbb{1}_{C_j}(\mathbf{x})$ directly by $P(\mathbf{x} \in C_j)$. However, it mixes several physical regimes, leading potentially to unphysical predictions, and can amplify the extrapolation of the reduced coordinates near the boundary decision. For these reasons, a hard-split approach has been selected.

The decision boundary in the input space parameters poses another problem. The classification is very prone to errors in this region. Indeed, the localization of the decision boundaries is subject to local variations, such as the choice of the supervised learning method (model-based, local methods, etc.) or the location of the training samples. Moreover, the reduced coordinates can be in extrapolation in this region. To overcome these problems, the classical model is employed for the predicted points near the interface.

IV. Numerical Results

A. Error Measurements

The classical method and the proposed LDM are assessed in this part with the RAE2822 airfoil [21,51]. It may be noted that an

additional study has been performed on the Burgers’ problem. The results are shown in the Supplemental Material burgers_am.pdf. The flow around the two-dimensional transonic airfoil is computed with a Navier–Stokes solver, involving a turbulence model. It is a challenging application in terms of surrogate modeling with high discontinuities due to the appearance of shocks. A three-dimensional input space is considered.

Particular attention is paid to the process of the input space decomposition and to the comparison of both classical approach and LDM in terms of accuracy. Several quantities are introduced to measure the accuracy. The so-called predictivity coefficient Q_2 gives the ratio of the output variance, which is explained by the metamodel. It can be interpreted as the classical coefficient of determination of the linear regression applied to a test sample [55]. The more the value is close to 1, the higher variance is explained by the model. It is expressed as:

$$Q_2^{(i)} = 1 - \frac{\sum_{j=1}^m [f^{(i)}(\mathbf{x}_{p_j}) - \tilde{f}^{(i)}(\mathbf{x}_{p_j})]^2}{\sum_{j=1}^m [\tilde{f}^{(i)}(\mathbf{x}_{p_j}) - f^{(i)}(\mathbf{x}_{p_j})]^2} \quad (29)$$

The root mean square error (RMSE) and the normalized root mean square error (NRMSE) are also introduced:

$$\text{RMSE}^{(i)} = \sqrt{\frac{1}{m} \sum_{j=1}^m [f^{(i)}(\mathbf{x}_{p_j}) - \tilde{f}^{(i)}(\mathbf{x}_{p_j})]^2} \quad (30)$$

$$\text{NRMSE}^{(i)} = \frac{\text{RMSE}^{(i)}}{f_{\max} - f_{\min}} \quad (31)$$

where f_{\max} and f_{\min} refer, respectively, to the scalar maximum and minimum values taken by the function to predict f for all the snapshots and over the mesh:

$$\begin{aligned} f_{\max} &= \max(\|f(\mathbf{x}_{p_1})\|_{\infty}, \dots, \|f(\mathbf{x}_{p_m})\|_{\infty}) \\ f_{\min} &= \min(\|f(\mathbf{x}_{p_1})\|_{\infty}, \dots, \|f(\mathbf{x}_{p_m})\|_{\infty}) \end{aligned} \quad (32)$$

One can note that the $Q_2^{(i)}$ and $\text{NRMSE}^{(i)}$ are computed at a given index i of the spatial domain Γ . The global measures are provided by averaging the quantities over this domain. The global quantities are referred to as $\langle Q_2 \rangle_{\Gamma}$ and $\langle \text{NRMSE} \rangle_{\Gamma}$, with $\langle \cdot \rangle_{\Gamma}$ the spatial average operator. However, in order to provide also a statistical error analysis, the averaged normalized error E_i is introduced. It corresponds to the absolute error between the exact value and the prediction, normalized by the range of variation, at snapshot level j :

$$E_j = \frac{\|f(\mathbf{x}_{p_j}) - \tilde{f}(\mathbf{x}_{p_j})\|_{\Gamma}}{f_{\max} - f_{\min}}, \quad \forall j \in [1, m] \quad (33)$$

The statistical distribution of E_i is presented with a box plot formalism. A box plot groups the data through different quantiles: the bottom and the top of the box represent, respectively, the value of the first and third quartiles, whereas the horizontal line inside the box is the median (second quartile) and the diamond the mean. The vertical lines indicate the data between the 5th percentile and the 1st quartile and between the 3rd quartiles and the 95th percentile. Finally the outliers are plotted as dots.

Besides the direct assessment of the surrogate model using a wide validation test, an estimation of the error can be provided only with the training set. Cross-validation strategies, such as the leave-one-out error, or the variance given by the Gaussian processes can estimate the a priori quality of each prediction. An example of application of these methods can be found in [56].

B. Two-Dimensional RAE2822 Transonic Airfoil

The viscous and turbulent flow around an RAE2822 airfoil has been widely studied in the literature both numerically and

experimentally [57,58]. The feature of prime interest of this test case is that the inflow conditions govern the flow regime, leading to the appearance of shock waves on the suction side. The detection and the clear separation of these regimes represent the main challenge for the model, demonstrating the capability of the LDM to deal with real and complex physics compared with the classical method.

1. Computational Configuration

The high-fidelity computations are carried out using the cell-centered finite-volume solver *elsA-ONERA* [59]. It has been developed at ONERA and solves the compressible Reynolds-averaged Navier–Stokes (RANS) equations on structured grids. From the numerical point of view, the classical second-order central scheme of Jameson et al. [47] is used for the space discretization. The time integration is performed with the backward Euler implicit scheme: the algebraic system is linearized with the LU-SSOR implicit method [60]. The turbulence modeling is ensured by the model of Spalart and Allmaras. A 2D mesh containing 23,010 points is used, as illustrated in the Fig. 4a. This test case has been successfully validated on a well-known regime flow [57] (Fig. 4b). The chord of the airfoil is written C , X refers to the horizontal coordinate, and Y refers to the vertical coordinate.

2. Input Parameter Space, Quantities of Interest, and Settings of the Surrogate Model

Three freestream parameters are considered as varying for this application: the flight speed, the angle of attack α , and the altitude h . Their variations are resumed in Table 1. These dimensional parameters are nondimensionalized and are expressed, respectively, as the Mach number M , angle of attack α (no change), and Reynolds number. One can note that the latter is impacted by the altitude variations but ensured to be maintained in a given interval in order to have a sufficiently resolved boundary layer. The atmosphere is modeled by the International Standard Atmosphere of the International Civil Aviation Organization [61]. It assumes that the air is a perfect gas and that the atmosphere can be divided into layers with a linear distribution of temperature against the altitude. The temperature T and the density ρ can be directly expressed in function of the altitude:

$$T = T_0 - Lh \quad (34)$$

$$\rho = \frac{p_0(1 - (Lh/T_0))^{g/rL}}{r(T_0 - Lh)} \quad (35)$$

with p_0 and T_0 the pressure and temperature at sea level, L the temperature lapse rate, r the specific gas constant of air, and g the

Table 1 Freestream conditions

Freestream variable	Amplitude of variation
Flight speed, m/s	88.5–269
Angle of attack, deg	0.5–3.0
Altitude, m	1000–11,000

acceleration due to the gravity. The quantities of interest of the simulation are the pressure coefficient C_p and the friction coefficient C_f on the suction side defined by

$$C_p = \frac{p - p_\infty}{(1/2)\rho_\infty U_\infty^2} \quad (36)$$

$$C_f = \frac{\tau_w}{(1/2)\rho_\infty U_\infty^2} \quad (37)$$

where p is the static pressure; τ_w is the wall shear stress; and p_∞ , ρ_∞ , and U_∞ are, respectively, the static pressure, the density, and the velocity in the freestream.

As regard the DOE, 30 samples of an Halton sequence form the training set, following the rule of thumb $10d$ [30]. The sampling of the LDM is divided into two parts. An initial DOE mixing subsonic and transonic snapshots explores uniformly the parameter space with an Halton sequence of 15 samples. The last 15 samples follow the resampling process described in the previous section. The flow is assumed to be driven by two different flow regimes. Therefore, the number of clusters is set to two for the clustering step. A test set has been built from 300 snapshots of a Sobol sequence in order to assess the LDM.

3. Analysis of the Surrogate Model Building Process

The two training sets exhibit interesting differences. The Halton approach explores uniformly the full input space, whereas the resampling process focuses on a low-dimensional high Mach number region, as depicted in Fig. 5 for the C_p . Indeed, the clustering phase automatically identifies the subsonic and the transonic snapshots thanks to the shock sensor. The supervised algorithm decomposes the input space parameter, allowing to determine the separation of the two physical regimes in the input parameter space, as illustrated in the Fig. 6 with both the training and testing sets. These two clusters can be interpreted as the subsonic and the transonic regions. It can be observed that the boundary is mainly influenced by the Mach number but also slightly by the angle of attack. Thus, the resampling process has increased the density of samples in the transonic regime, improving the accuracy of the model where the predictions are more

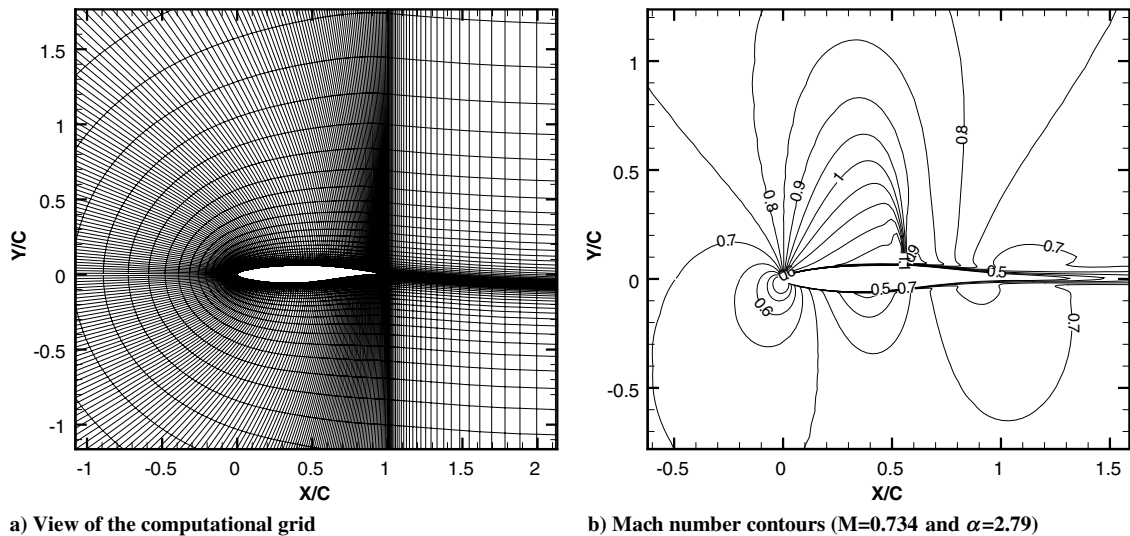


Fig. 4 Flow around the RAE2822 airfoil.

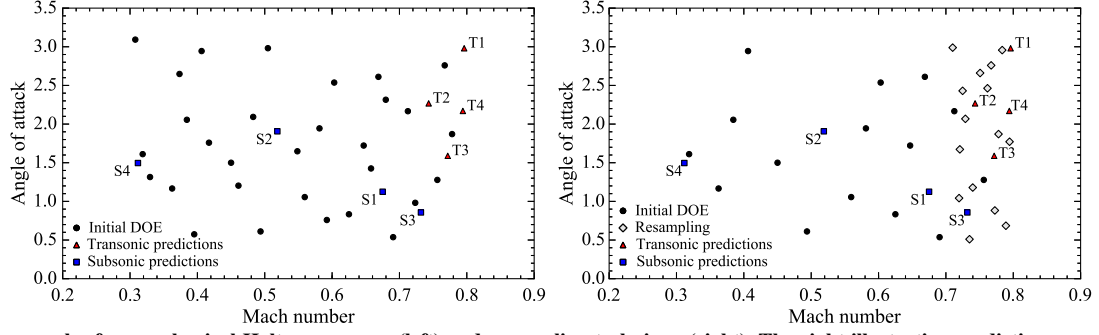


Fig. 5 Thirty samples from a classical Halton sequence (left) and resampling technique (right). The eight illustrative predictions are also identified (with blue squares and red triangles).

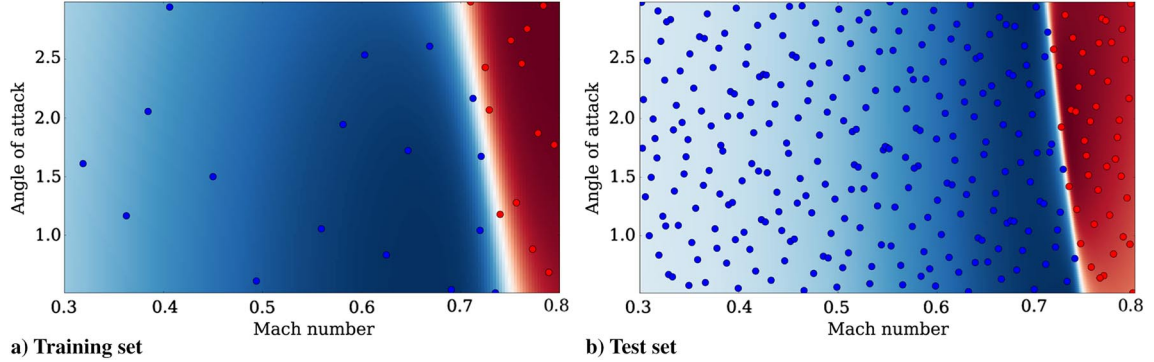


Fig. 6 Input space decomposition. Each color corresponds to a cluster: the blue one is the subsonic regime and the red one is the transonic regime.

challenging. One can note that the boundary region is well defined by a thin region of probability between 40 and 60%.

The model can also be analyzed from a dimension reduction point of view with Table 2. For a given POD energy ratio of 0.99%, the classical method reduces the dimension of the 30 snapshots with 10 modes and an entropy of 0.37, whereas the LDM identifies clearly a POD basis with a low entropy and a POD basis with a large one. The highest nonlinear cluster shows an entropy value of 0.63, 70% bigger than the linear cluster and the classical method. It means that the data of the subsonic POD basis and of the classical method can be highly compressed. Conversely, the transonic POD basis requires 9 modes for 13 snapshots. Thus, the active resampling provides extra nonredundant information to the LDM compared with the classical method.

The shape of the modes can also help to understand the behavior of the different models. As regard the classical method, only discontinuous features emerge clearly from the global POD as illustrated in Fig. 7a, where POD modes shown only dominant discontinuities and non-moving shocks. Therefore all the reduced coordinates associated with subsonic snapshots must exactly cancel out the discontinuities of the modes. For this reason, the prediction of the reduced coordinates for snapshots in the subsonic region can be sensitive to interpolation errors leading to the appearance of “residual” shocks. Thus, the clear separation of the regimes in the POD domain represents a major asset inherent in the LDM. Figure 7b shows the first three modes of the two POD bases. High nonlinearities arises for the transonic regime, whereas the subsonic region highlights similarities with the modes of the classical method. The only difference is that the subsonic modes are smoother.

Table 2 Required modes of the different methods for the RAE2822

Method	Number of snapshots	Number of modes	Entropy
Classical	30	7	0.37
LDM (transonic regime)	13	9	0.63
LDM (subsonic regime)	17	6	0.36

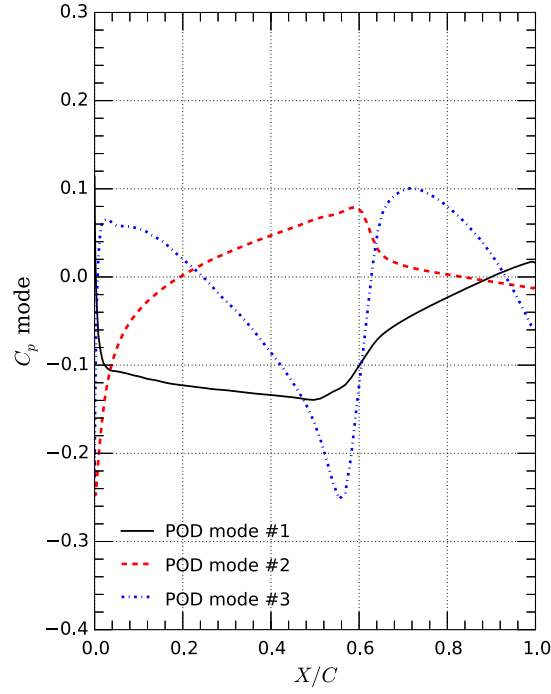
These statements are confirmed by looking at C_p profiles, comparing classical and LDM methods. Eight predictions have been computed for an illustrative purpose and are grouped by physical regime (S for subsonic and T for transonic). Their coordinates in the parameter space are summarized in the Table 3 and their repartition is illustrated in Fig. 5. One can observe that for the subsonic regime in Fig. 8, the classical method induces residual shocks, certainly due to errors of prediction on the reduced coordinates coupled with sharp POD modes not adapted to subsonic flows. On the contrary, the residual shocks are filtered by the LDM as lower discontinuities are present in the training snapshots building the POD basis. It leads to final predictions less sensitive to errors on the reduced coordinates. As regard C_p profiles shown in the transonic regimes in Fig. 9, the LDM shows improved accuracy. In particular, the modeling of the shock waves gives an insight into the behavior of the two models. Significant discrepancies in terms of shock displacement and shock amplitude occur for the classical POD/GPR method. Indeed, the combination of angle of attack and Mach number influences directly the localization of the steady shock wave and its amplitude. However, this behavior can be accurately caught only if the training set contains a sufficient amount of snapshots with shocks, which is not the case for the classical POD/GPR methods. The same trend is observed for the C_f profiles in Figs. 10 and 11.

4. Accuracy of the Model

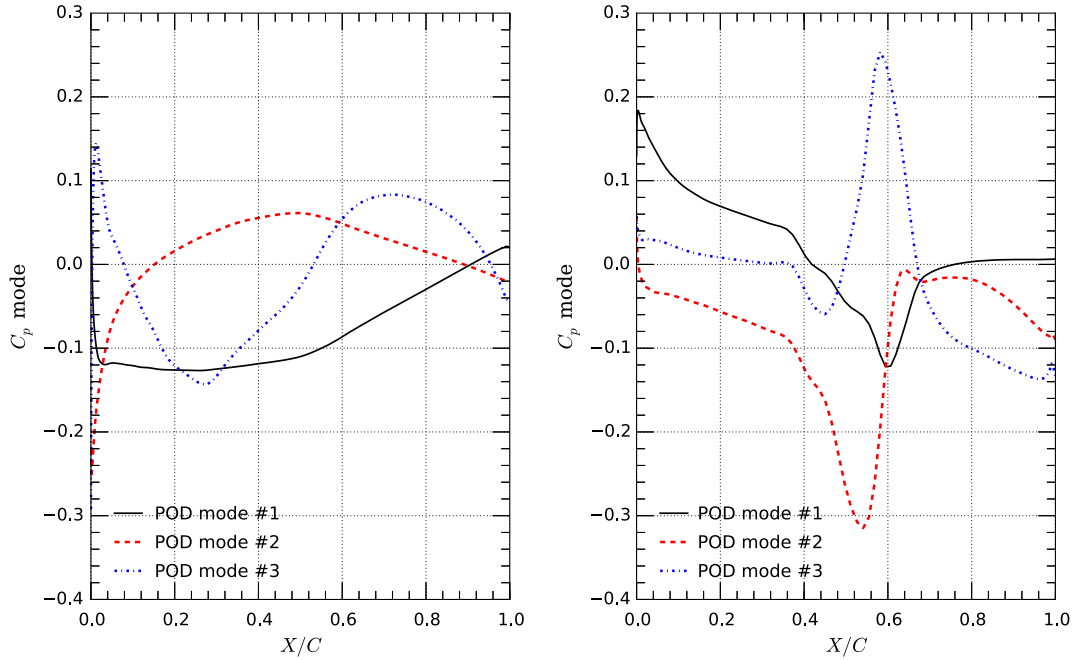
In this section, a more detailed look is given to the analysis of the model accuracy. Figure 12 displays the comparison of the normalized error in terms of C_p and C_f for both methods between the predictions and the test set. The results are presented with a box plot formalism and three different phases have been considered:

- 1) The full domain contains all the samples of the testing set.
- 2) The subsonic regime is only composed of the testing samples identified as subsonic, in blue dots in Fig. 6b.
- 3) The transonic regime encompasses the other snapshots, shown as red dots in Fig. 6b.

A significant improvement in the accuracy is induced by the LDM for the C_p . As regard the full domain, the normalized error decreases dramatically for all the statistical characteristics of the box plot.



a) POD modes for the classical method



b) POD modes of the C_p for the LDM, subsonic (left) and transonic (right)

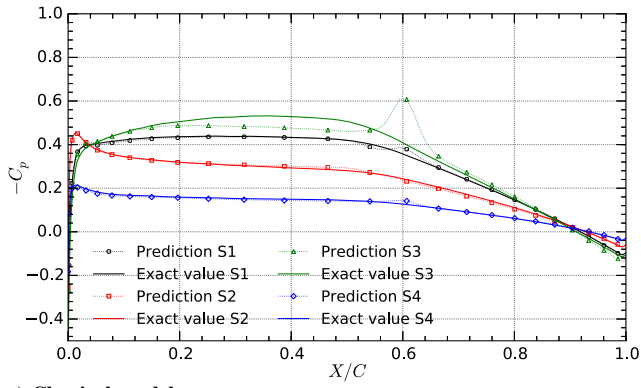
Fig. 7 POD modes of the RAE2822 simulations.

Table 3 Coordinates in the parameter space of the eight illustrative predictions

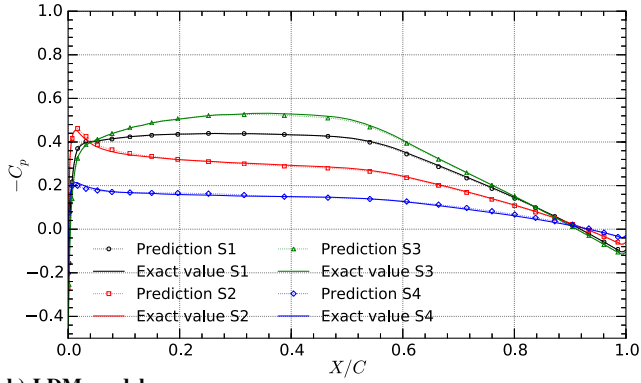
Predictions	Mach number	Angle of attack, deg	Altitude, m
S1	0.675	1.125	8500
S2	0.519	1.906	1625
S3	0.722	1.047	1937
S4	0.312	1.496	5453
T1	0.796	2.980	6391
T2	0.743	2.267	10,102
T3	0.772	1.589	3168
T4	0.794	2.170	3617

In particular, the extreme value of the LDM reaches the same level as the 95% error of the classical method, illustrating a large reduction of the model variability. The box plots for subsonic and transonic regimes provide a closer look at the repartition of the error. It clearly appears that the LDM improves the predictions at transonic regime, explained by the increase of the sample density. On the other hand, the subsonic regime is very slightly impacted compared with the classical method, although samples have been removed.

Table 4 provides a more global view of the error with the spatial average of the Q_2 and NRMSE. Whatever the quantity measuring the error, the same trend is observed for the two quantities of interest: the LDM significantly improves the accuracy of the predictions

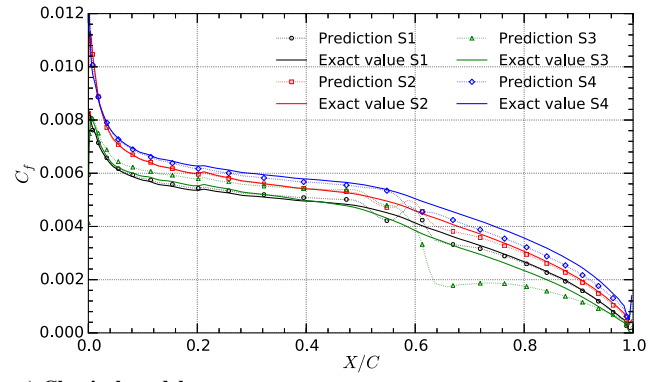


a) Classical model

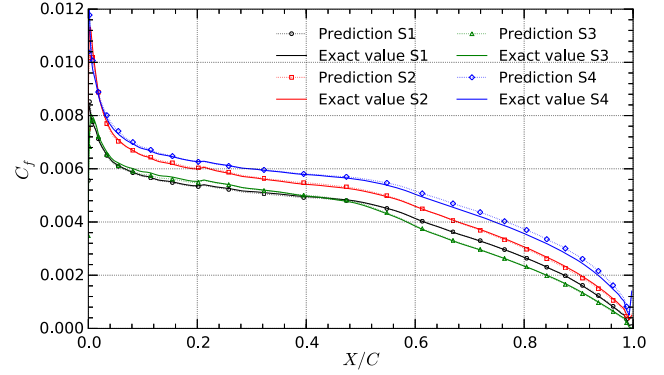


b) LDM model

Fig. 8 C_p profiles in the subsonic regime.

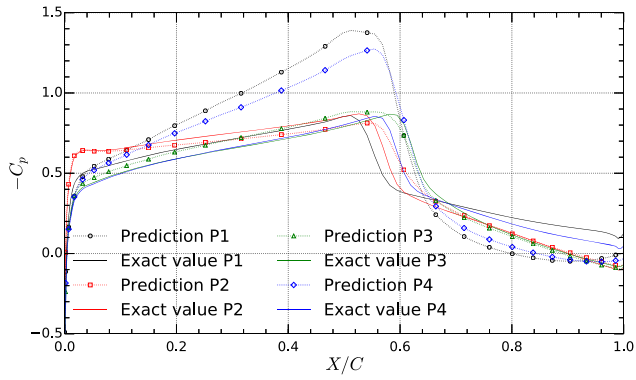


a) Classical model

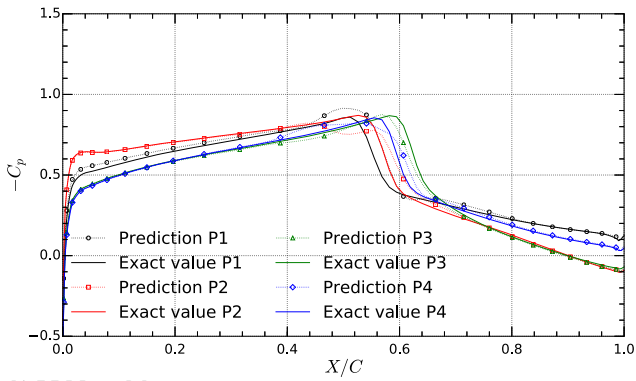


b) LDM model

Fig. 10 C_f profiles in the subsonic regime.

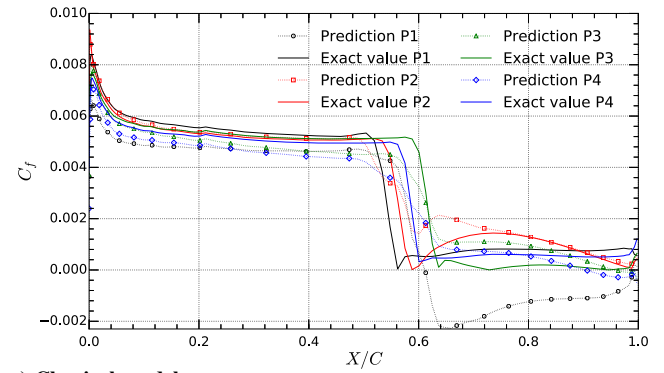


a) Classical model

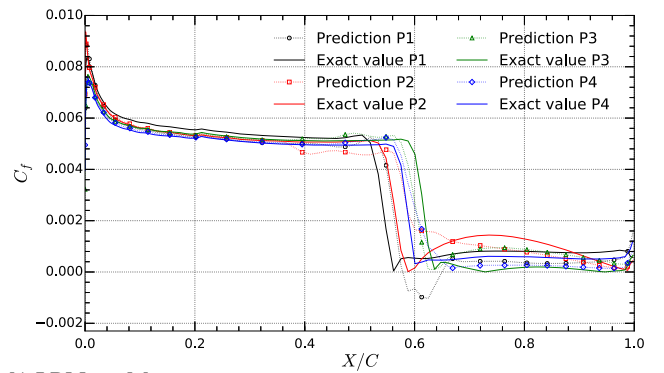


b) LDM model

Fig. 9 C_p profiles in the transonic regime.



a) Classical model



b) LDM model

Fig. 11 C_f profiles in the transonic regime.

compared with the classical method. There are, however, legitimate doubts as to the value of the $\langle Q_2 \rangle_\Gamma$ for the C_f , which is below zero for the transonic regime. Several explanations can be given. First of all,

the $\langle Q_2 \rangle_\Gamma$ is spatially averaged and the value of C_f can be very close to zero after the shock. Thus, some values of Q_2 fall far below zero in this region, impacting directly the average of the predictivity

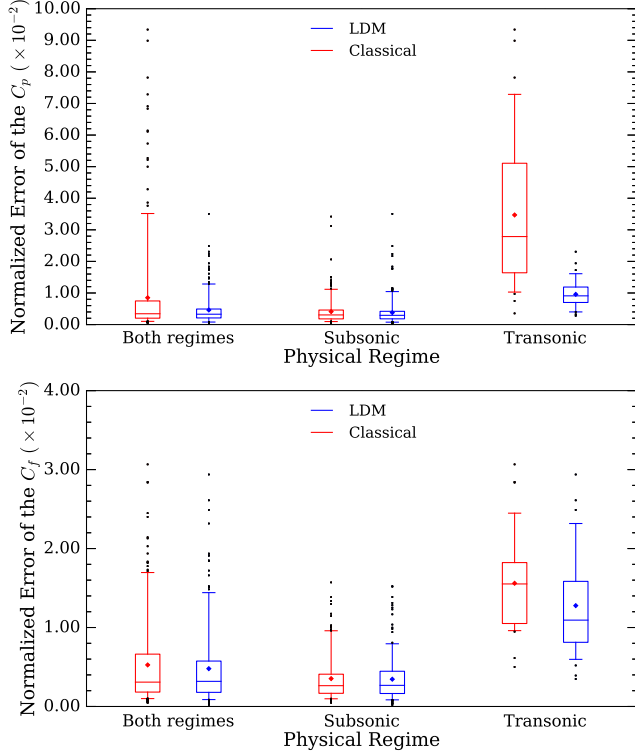


Fig. 12 Accuracy of the surrogate model in terms of C_p and C_f .

coefficient. Then, the skin friction coefficient is also more challenging to predict due to its higher dependency on the altitude and higher nonlinearity.

Finally, the evolution of the NRMSE with the number of training samples is shown in Fig. 13 for both the pressure and skin friction coefficients. One may note that the classical method with 50 training samples has broadly the same error than the LDM strategy with 30 samples. In the end, this observation could be seen as a saving of the computational budget of more than 60%. Moreover, the error of the model seems to continuously decrease when the number of training samples increases.

V. Conclusions

The aim of this paper was to build a nonintrusive reduced order model capable of coping with aerodynamics problems at multiple operating conditions. These latter involve hyperbolic equations and different physical regimes leading to discontinuous features of solutions. The original local decomposition method (LDM) strategy alleviates the issues encountered by the classical method using global proper orthogonal decomposition (POD) and multiparameter interpolation in order to solve the regression problem. The LDM consists of building a local reduced order model for each physical regime. This approach has been developed to be more suited to hyperbolic properties than the global POD expansion. The decomposition of the problem into several local reduced order models is achieved using machine learning methods. Two major steps are associated with the LDM strategy: the use of a Jameson's shock sensor enhancing the physical regime recognition in order to ease the clustering of the problem and an active sampling adding automatically extra information to the subspaces with the highest discontinuous structures. The LDM has been assessed on an analytical moving shock problem and the simulation of a turbulent flow around the transonic RAE2822 airfoil. The results reveal a significant improvement of the model accuracy, especially in the regions of high gradients and discontinuities.

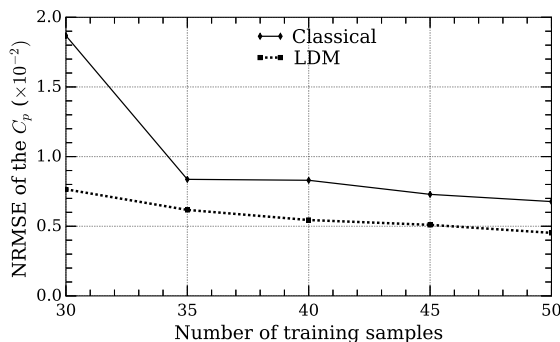
Further work is needed to increase the efficiency of the strategy. First, the resampling technique has to be improved. The snapshots added to a specific subspace come from the continuation of a low-discrepancy sequence. For example, a method minimizing the variance of the Gaussian process regression could be considered. Moreover, the new snapshots are computed sequentially as the probability of belonging to each subset is updated at each iteration. A new process of parallelization should be devised to take advantage of high-performance computing during the iterative sampling step by combining multiple simultaneous jobs into large ensembles. Second, the extrapolation at the interface of the input space parameter remains an open issue. Further applications of the LDM strategy are expected on three-dimensional flows for industrial aerodynamic applications. Especially, it is planned to evaluate this method in a mission analysis context, taking advantage of the results obtained for the transonic regions.

Acknowledgments

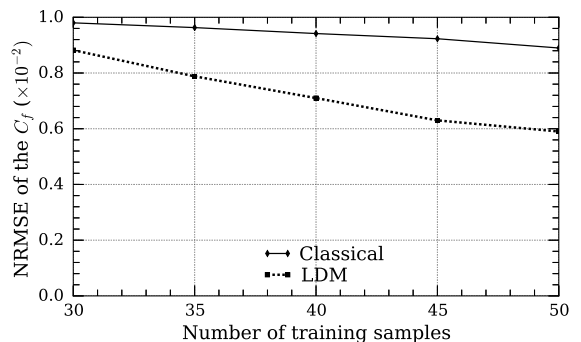
This work is part of the MDA-MDO project of the French Institute of Technology IRT Saint Exupéry. We wish to acknowledge the PIA

Table 4 Summary of the results in terms of Q_2 and NRMSE for the RAE2822

Regime	Method	$\langle Q_2 \rangle_\Gamma$ of C_p	$\langle \text{NRMSE} \rangle_\Gamma$ of C_p	$\langle Q_2 \rangle_\Gamma$ of C_f	$\langle \text{NRMSE} \rangle_\Gamma$ of C_f
Both	Classical	0.897	1.93×10^{-2}	0.837	1.15×10^{-2}
	LDM	0.989	7.48×10^{-3}	0.908	9.53×10^{-3}
Subsonic	Classical	0.984	7.46×10^{-3}	0.912	6.61×10^{-3}
	LDM	0.990	6.31×10^{-3}	0.957	6.72×10^{-3}
Transonic	Classical	0.0974	4.64×10^{-2}	-0.303	2.54×10^{-2}
	LDM	0.901	9.79×10^{-3}	-0.0223	1.72×10^{-2}



a) Pressure coefficient



b) Friction coefficient

Fig. 13 Evolution of the NRMSE with the number of training samples.

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